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This is a pre-print of the following article

Original Citation:

Adhesion of surfaces with wavy roughness and a shallow depression / Papangelo, A.; Ciavarella, M.. - In: MECHANICS OF MATERIALS. - ISSN 0167-6636. - STAMPA. - 118:(2018), pp. 11-16. [10.1016/j.mechmat.2017.12.005]

Availability:

This version is available at <http://hdl.handle.net/11589/125057> since: 2022-06-08

Published version

DOI:10.1016/j.mechmat.2017.12.005

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Adhesion of surfaces with wavy roughness and a shallow depression

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Abstract

Recently, a simple and elegant "dimple" model was introduced by McMeeking *et al.* (Adv Eng Mat 12(5), 389-397, 2010) to show a mechanism for a bistable adhesive system involving a surface with a shallow depression. The system shows, at least for intermediate levels of stickiness, that external pressure can switch the system into a "strong adhesive" regime of full contact, or into weak adhesion and complete pull-off, similarly to the contact of surfaces with a single scale of periodical waviness. We add to this model the effect of roughness, in the simple form of axisymmetric single scale of waviness, permitting a very detailed study, and we show that this induces a resistance to jumping into full contact on one hand (limiting the "strong adhesion" regime), and an enhancement of pull-off and of hysteresis starting from the partial contact state on the other (enhancing the "weak adhesion" regime). We show the system depends only on two dimensionless parameters, depending on the ratio of work of adhesion to the energy to flatten the dimple or waviness, respectively. The system becomes pressure-sensitive also in the intermediate states, as it is observed in real adhesive rough systems. The model obviously is specular to the Guduru model of rough spheres (Guduru, JMPS, 55, 473-488, 2007), with which it shares the limitations of the analysis assuming a connected contact (crack) area, and serves also the purpose of showing the effect of a depression into an otherwise periodic rough contact, towards the understanding of adhesion with multiple scales of roughness.

Keywords:

Roughness, Adhesion, dimple model, JKR adhesion

1. Introduction

Adhesion in the presence of roughness is usually destroyed very easily, as it was proved by Fuller and Tabor (1975), even in low modulus materials like smooth rubber lenses against roughened surfaces. Therefore, it is still surprising that some insects use adhesion for their locomotion, by using a series of mechanisms, the study of which has generated a very important area of research in the last decades. The mechanisms include splitting the contact into many spots and optimizing the shape and size of each contact (Hui *et al.* 2004, Kamperman *et al.*, 2010, Gao & Yao 2004). However, even the best of the mechanisms, is unlikely to work with all possible rough surfaces, showing wavelengths and amplitude over different length scales (Huber *et al.*, 2007, Pugno & Lepore, 2008), showing a truly efficient system for multiscale arbitrary roughness is extremely difficult to achieve. The understanding about when adhesion can be very strong or very weak depending on features of roughness, pre-load, and system architecture is so far very remote from being complete.

At the opposite end of the classical finding of Fuller & Tabor (1975), Johnson (1995) demonstrated a mechanism for which roughness in the form of a sinusoidal wave, has a *minimal effect* after a sufficiently high pressure has been applied, because the contact naturally jumps into a state of full contact. Indeed, this can happen even *spontaneously* (at zero external load) for sufficiently high work of adhesion. After this state has been reached, virtually the theoretical strength of the material is found, and one has to postulate either a tiny flaw at the interface, or air entrapment to escape this limit which is far from common experience. Therefore, the role of roughness can be pressure-sensitive.

Guduru (2007) found a mechanism of enhancement which has some connection with Johnson's model, in that he imagined a sphere with roughness in the form of axisymmetric waviness, and solved the problem assuming that roughness was effectively flattened during the deformation, so the contact was a simply connected area. This results in very large oscillations in the normal load as a function of indentation, which were also observed experimentally in Guduru & Bull (2007), and gave rise to both large dissipation because of multiple jumps from unstable to stable branches, and to an enhancement of pull-off. Kesari & Lew (2010) further discussed how these unstable jumps could in the limit of small wavelength roughness define a continuous curve

removing the oscillations of the original solution: Ciavarella (2016a) further remarked that the Kesari & Lew (2010) asymptotic expansion corresponds to splitting the classical JKR theory solution for spheres given in (Johnson *et al.*, 1971) into two branches, loading and unloading ones, which correspond to an decreased and increased values of work of adhesion, respectively, uniquely dependent on the Johnson (1995) parameter for sinusoidal waviness contact. Ciavarella (2016b) further used the Kesari & Lew (2010) asymptotic expansion for multiscale roughness in the form of a Weierstrass function, showing that the enhancement could be extremely large in this case, although the assumptions of the simply connected area solution become increasingly stretched.

Recently, McMeeking *et al.* (2010) have proposed a very simple model where two surfaces are gently brought into contact, one of which having a single small depression. This is in a sense a simplification of the single scale of waviness of Johnson’s (1995) model, with the additional significant advantage that in full 3D situations, sinusoidal roughness leads in intermediate regimes to a very complex problem with non-circular contact areas, whereas the dimple model preserves axisymmetry and permits a very simple solution, particularly with the shape chosen by McMeeking *et al.* The model however preserves all of the features of the periodic waviness problem, in that there is a possibility of jump-into contact at some level of compression (or it can be spontaneous for sufficient level of adhesion), and that there is an unstable pull-off at some value of external tension. This pull-off is no longer occurring on the crests, and therefore is not the known value for spheres given by JKR theory (Johnson *et al.*, 1971), but depends on the shape of the depression.

As Johnson (1995) remarked, the single scale waviness model shows an extreme behaviour, which is likely to be affected by deviation due also to the presence of finer-scale roughness. Guduru’s model already answers some questions about the case of two scales of waviness, for contact near the crest, but the spherical geometry doesn’t admit a ”full contact” limit, and therefore it doesn’t address the problem towards this regime. Instead, the simple dimple model of McMeeking *et al.* (2010) is ideal to a quantitative assessment of the full problem, by adding axisymmetric roughness. In other words, despite idealized, this geometry can be a model for two scales of roughness both in what happens in a single scale of waviness when encountering a depression in a surface, or specularly, for the depression itself having roughness. The advantage of the model is that we can study it in great details, especially in the asymptotic regime in which the wavelength of the roughness is much

smaller than the non-contact area. We hope to elucidate qualitatively some features of the general behaviour of adhesive surfaces.

2. Formulation

We consider as smooth geometry that of a surface with a shallow depression, in the form of a dimple of amplitude δ_0 and radius b (McMeeking *et al.* 2010), defined as

$$\delta = \frac{2}{\pi} \delta_0 E\left(\frac{r}{b}\right), \quad \frac{r}{b} \leq 1 \quad (1)$$

$$\delta = \frac{2}{\pi} \delta_0 \frac{r}{b} \left[E\left(\frac{r}{b}\right) - \left[1 - \left(\frac{b}{r}\right)^2 \right] K\left(\frac{b}{r}\right) \right], \quad \frac{r}{b} > 1 \quad (2)$$

where K, E are complete elliptic integrals of first and second kind. To the smooth geometry, we add an axisymmetric sinusoidal roughness of amplitude and wavelength g, λ .

The geometry is clarified in Fig.1.

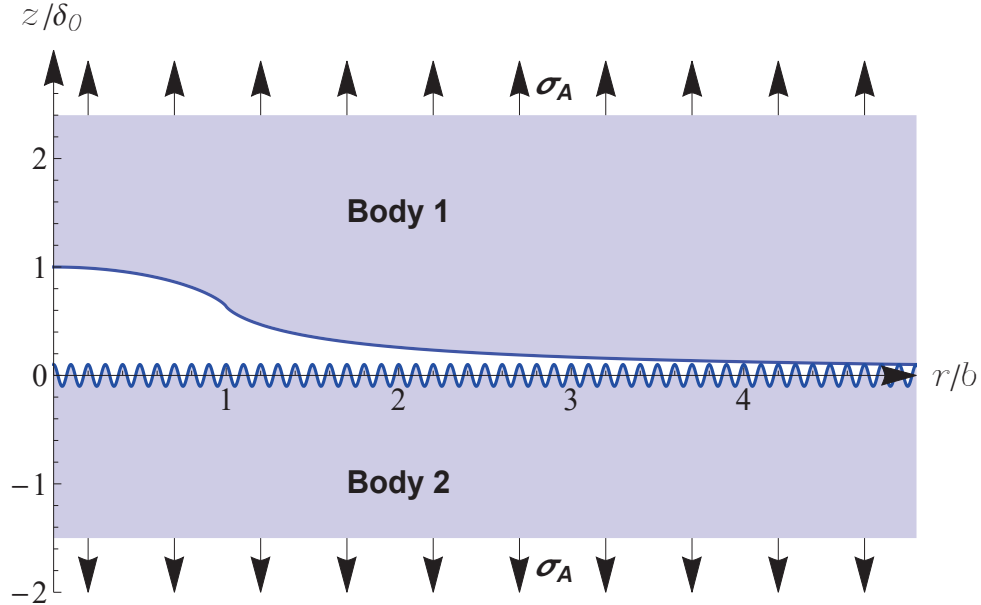


Fig.1 Geometry of the system. A flat surface having a shallow depression in the form of a "dimple" – against a surface with wavy roughness (roughness could be added to either of the surfaces).

The system will tend to adhere from the remote points towards the center, and therefore, assuming the contact is continuous (which requires roughness is not too large, see Discussion), the contact correspond to a classical penny-shaped crack. Using superposition principles, we can solve for the penny-shaped crack under internal tension, given by the state of stress induced in the full adhered state. The latter is defined by the combination of 3 components:

- (i) the localized tensile stress T in $r < b$, i.e. inside the dimple

$$T = \frac{E^* \delta_0}{2b}, \quad r < b \quad (3)$$

- (ii) a remote tension σ_A in the entire plane, and
- (iii) a sinusoidal variation

$$\sigma_{rough} = p^* \cos \frac{2\pi r}{\lambda} \quad (4)$$

where $p^* = \pi E^* g / \lambda$. Notice this is a plane strain approximation, which is proven to be extremely good for our scopes in Appendix.

Using the standard results for axisymmetric cracks (see eg. Maugis, 2000) under internal pressure $p(r)$, for a crack of radius c , we derive the stress intensity factor as (Maugis, 2000, 3.117)

$$K_I = \frac{2}{\sqrt{\pi c}} \int_0^c \frac{sp(s) ds}{\sqrt{c^2 - s^2}} \quad (5)$$

The first two components (i-ii) give

$$K_I = (\sigma_A + T) \frac{2\sqrt{c}}{\sqrt{\pi}}, \text{ for } c < b \quad (6)$$

$$= \frac{2}{\sqrt{\pi c}} \left[\sigma_A c + T \left(c - \sqrt{c^2 - b^2} \right) \right], \text{ for } c > b \quad (7)$$

The third component (iii) gives

$$K_I = \frac{2p^*}{\sqrt{\pi c}} \int_0^c \frac{s \cos \frac{2\pi s}{\lambda} ds}{\sqrt{c^2 - s^2}} = p^* \sqrt{\pi c} H_{-1} \left(\frac{2\pi c}{\lambda} \right) \quad (8)$$

where H_{-1} is the Struve function of order -1.

Under the assumptions of Linear Elastic Fracture Mechanics (often in adhesion, called "JKR" regime, from Johnson *et al.*, 1971), equilibrium is obtained equating the total K_I to the K_{Ic} toughness of the material pair, or equivalently the energy release rate to the work of adhesion $G = w$ where $2E^*w = K_{Ic}^2$. Hence we obtain from (6, 7, 8)

$$K_{Ic} = (\sigma_A + T) \frac{2\sqrt{c}}{\sqrt{\pi}} + p^* \sqrt{\pi c} H_{-1} \left(\frac{2\pi c}{\lambda} \right), \text{ for } c < b \quad (9)$$

$$K_{Ic} = \frac{2}{\sqrt{\pi c}} \left[\sigma_{Ac} + T \left(c - \sqrt{c^2 - b^2} \right) \right] + p^* \sqrt{\pi c} H_{-1} \left(\frac{2\pi c}{\lambda} \right), \text{ for } c > b \quad (10)$$

i.e.

$$\frac{\sigma_A}{T} = -1 - \frac{\pi p^*}{2T} H_{-1} \left(\frac{2\pi c}{\lambda} \right) + \frac{\pi K_{Ic}}{2T\sqrt{\pi c}}, \text{ for } c < b \quad (11)$$

$$\frac{\sigma_A}{T} = - \left(1 - \sqrt{1 - \left(\frac{b}{c} \right)^2} \right) - \frac{\pi p^*}{2T} H_{-1} \left(\frac{2\pi c}{\lambda} \right) + \frac{\pi K_{Ic}}{2T\sqrt{\pi c}}, \text{ for } c > b \quad (12)$$

One natural dimensionless parameter is then

$$\alpha_d = \frac{K_{Ic}\sqrt{\pi}}{2T\sqrt{b}} = \frac{\pi K_{Ic}}{2T\sqrt{\pi c}} \frac{\sqrt{c}}{\sqrt{b}} \quad (13)$$

which, by analogy with the sinusoidal case of Johnson (1995), we can define the Johnson parameter for the smooth dimple, proportional to the ratio between the work of adhesion, and the elastic energy to flatten the smooth dimple. Hence, we can restate the LEFM curves normalizing the stresses by T as $\hat{\sigma}_A = \frac{\sigma_A}{T}$ and $\hat{p}^* = \frac{p^*}{T}$, and all length scales by b as $\hat{c} = c/b$ and $\hat{\lambda} = \lambda/b$, obtaining

$$\hat{\sigma}_A = -1 - \frac{\pi \hat{p}^*}{2} H_{-1} \left(\frac{2\pi \hat{c}}{\hat{\lambda}} \right) + \frac{\alpha_d}{\sqrt{\hat{c}}}, \text{ for } \hat{c} < 1 \quad (14)$$

$$\hat{\sigma}_A = -1 + \sqrt{1 - \frac{1}{\hat{c}^2}} - \frac{\pi \hat{p}^*}{2} H_{-1} \left(\frac{2\pi \hat{c}}{\hat{\lambda}} \right) + \frac{\alpha_d}{\sqrt{\hat{c}}}, \text{ for } \hat{c} > 1 \quad (15)$$

Using the expansion of $H_{-1} \left(\frac{2\pi \hat{c}}{\hat{\lambda}} \right)$ for $\hat{\lambda} \rightarrow 0$, similarly to what done by Kesari & Lew (2011) for the problem of a rough sphere, we obtain the first

term as¹

$$H_{-1}\left(\frac{2\pi\widehat{c}}{\widehat{\lambda}}\right) \simeq \frac{1}{\pi} \sqrt{\frac{\widehat{\lambda}}{\widehat{c}}} \sin\left(\frac{\pi}{4} + \frac{2\pi\widehat{c}}{\widehat{\lambda}}\right)$$

and therefore, this function will have minima (and maxima) which can be joined, obtaining

$$\widehat{\sigma}_A^\pm = -1 \pm \frac{\widehat{p}^*}{2} \sqrt{\frac{\widehat{\lambda}}{\widehat{c}}} + \frac{\alpha_d}{\sqrt{\widehat{c}}}, \text{ for } \widehat{c} < 1 \quad (16)$$

$$\widehat{\sigma}_A^\pm = -1 + \sqrt{1 - \frac{1}{\widehat{c}^2}} \pm \frac{\widehat{p}^*}{2} \sqrt{\frac{\widehat{\lambda}}{\widehat{c}}} + \frac{\alpha_d}{\sqrt{\widehat{c}}}, \text{ for } \widehat{c} > 1 \quad (17)$$

Exactly as it happens for the rough sphere (see Ciavarella, 2016a, 2016b), we can group the terms corresponding to the smooth profile and the roughness induced first order increase, and accordingly define an increased/decreased work of adhesion for unloading/loading respectively. For the rough sphere, this results in JKR equations with different work of adhesion on loading and unloading. Here, this results in

$$\widehat{\sigma}_A^\pm = -1 + \frac{1}{\sqrt{\widehat{c}}} \left(\alpha_d \pm \frac{\widehat{p}^*}{2} \sqrt{\widehat{\lambda}} \right), \text{ for } \widehat{c} < 1 \quad (18)$$

$$\widehat{\sigma}_A^\pm = -1 + \sqrt{1 - \frac{1}{\widehat{c}^2}} + \frac{1}{\sqrt{\widehat{c}}} \left(\alpha_d \pm \frac{\widehat{p}^*}{2} \sqrt{\widehat{\lambda}} \right), \text{ for } \widehat{c} > 1 \quad (19)$$

Hence, effectively the curves are identical to those of the "smooth" dimple, where one substitutes α_d with

$$\alpha_{d,rough}^{loading} = \left(\alpha_d - \frac{\widehat{p}^*}{2} \sqrt{\widehat{\lambda}} \right) = \alpha_d \left(1 - \frac{1}{\sqrt{\pi\alpha}} \right) \quad (20)$$

$$\alpha_{d,rough}^{unloading} = \left(\alpha_d + \frac{\widehat{p}^*}{2} \sqrt{\widehat{\lambda}} \right) = \alpha_d \left(1 + \frac{1}{\sqrt{\pi\alpha}} \right) \quad (21)$$

where we have recognized $\alpha = \frac{2\alpha_d}{\widehat{p}^* \sqrt{\pi\widehat{\lambda}}}$ with α being exactly the parameter

¹This was obtained with some simple manipulations of the Mathematica command "Series".

introduced by Johnson (1995) for the roughness of a single sinusoid of wavelength and amplitude λ, g , defined as

$$\alpha^2 = \frac{2}{\pi^2} \frac{w\lambda}{E^*g^2} \quad (22)$$

Notice that while $\alpha_{d,rough}^{unloading}$ is always greater than the original α_d , $\alpha_{d,rough}^{loading}$ is always smaller, and indeed it can become negative (for $\alpha < 1/\sqrt{\pi} = 0.57$). This simply means that the curve for loading will not correspond to any physical curve for a smooth dimple, and in fact it is due to the fact that the pressure to reach full contact becomes even higher than that of the smooth dimple without adhesion.

3. Results

To elucidate the results, let us start by showing the curves for the "smooth" dimple, in Fig.2. In particular, Fig.2a shows various values of dimple parameter α_d , from zero (adhesionless contact), which requires a compression $\hat{\sigma}_A = -1$ to obtain full contact, to values higher than 1, which show no equilibrium points at zero external load – implying spontaneous jump into full contact. More precisely, considering the case $\alpha_d = 0.75$ plotted in Fig.2b, and starting from very large \hat{c} , equilibrium is achieved at point A. After that, if we load in compression, we move towards negative $\hat{\sigma}_A$ and jump into full contact at point B, as the branch with negative slope is unstable. From this full contact condition, only very high values of tension will detach the interface, of the order of theoretical strength. If, instead, from point B we start unloading, we enlarge the crack size until another instability is reached, that of pull-off at point C.

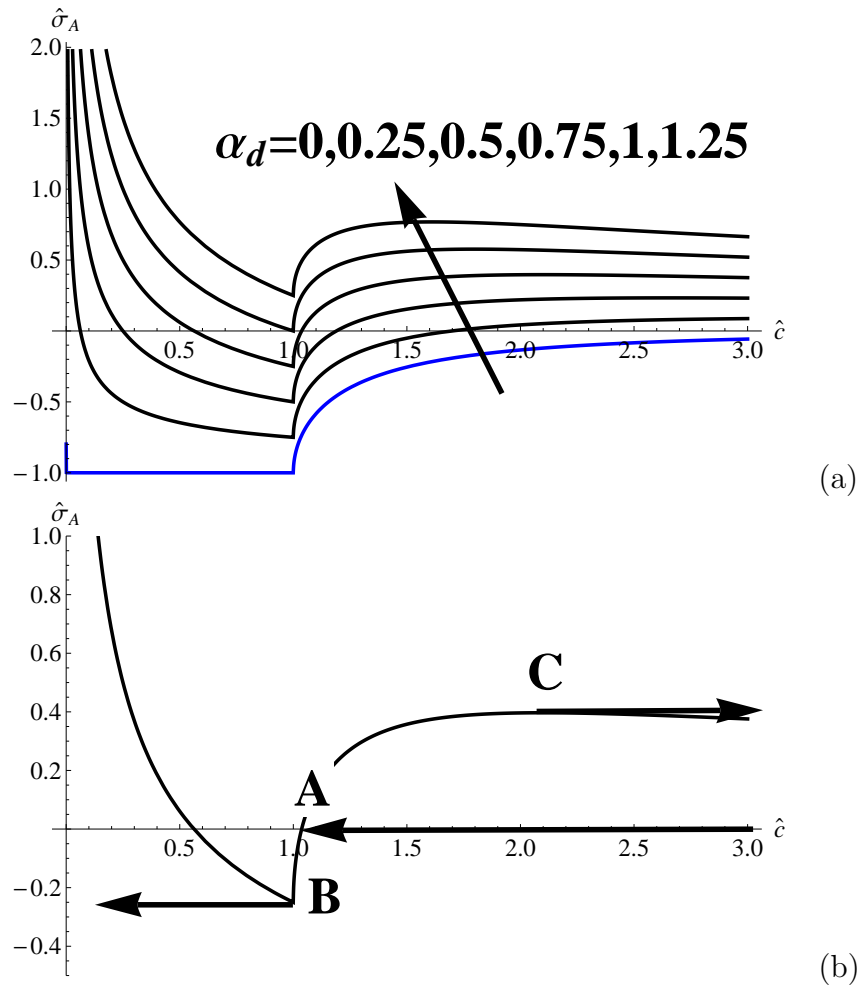
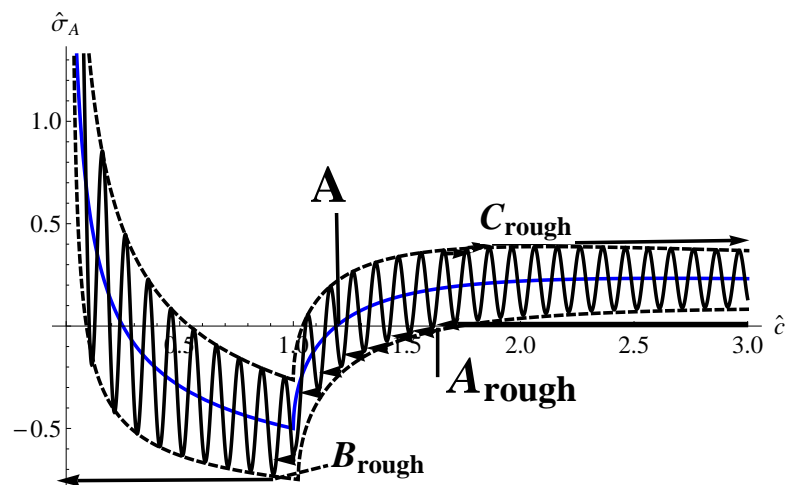
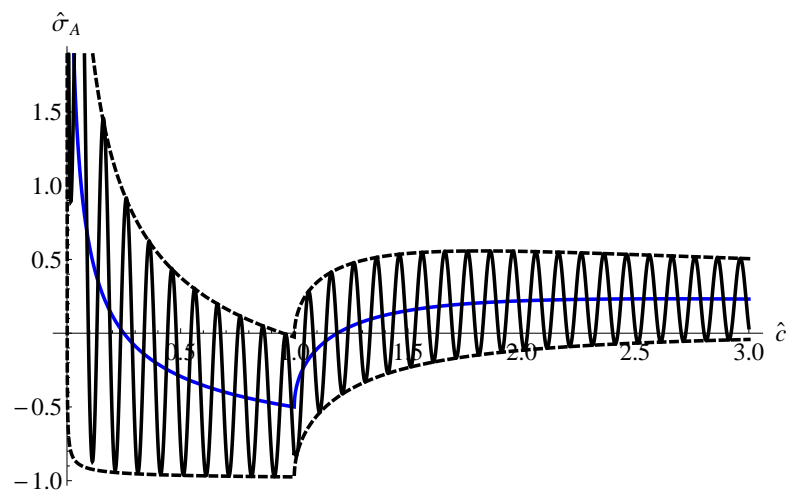


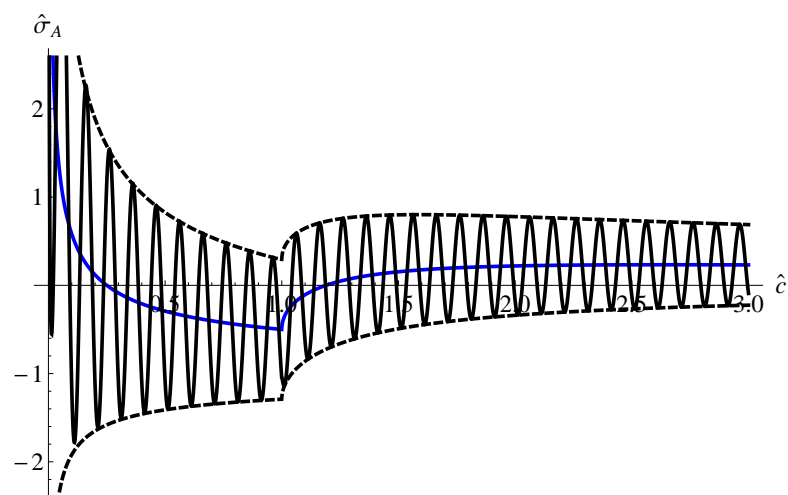
Fig.2 Example results for the smooth dimple, (a) with $\alpha_d = 0, 0.25, 0.5, 0.75$. and (b) for the case $\alpha_d = 0.75$ with various loading/unloading paths



(a)



(b)



(c)

Fig.3 Example results for the rough dimple $\alpha_d = 0.5, \hat{\lambda} = 0.1$. (a) $\hat{p}^* = 1.5$, (and hence $\alpha = 1.19, \alpha_{d,rough}^{loading} = 0.26, \alpha_{d,rough}^{unloading} = 0.737$); (b) $\hat{p}^* = 3$, (and hence $\alpha = 0.595, \alpha_{d,rough}^{loading} = 0.026, \alpha_{d,rough}^{unloading} = 0.97$); (c) $\hat{p}^* = 5$, (and hence $\alpha = 0.357, \alpha_{d,rough}^{loading} = -0.29, \alpha_{d,rough}^{unloading} = 1.29$)

Looking at the rough system, we show some examples in Fig.3, where we plot with solid blue line the smooth system, with dashed lines the "envelope" solutions (18, 19). Starting with Fig.3a, we have a system with $\alpha_d = 0.5, \hat{p}^* = 1.5, \hat{\lambda} = 0.1$ (and hence $\alpha = 1.19$) where we have evidenced with arrows the jumps of the system when it encounters an unstable branch of the solution. Clearly, the equilibrium crack size at zero external load, point A, has now moved to A_{rough} which corresponds to a larger size. Also, the jump into full contact B_{rough} , occurs for a much higher compressive stress than in the smooth case, and for a crack size slightly smaller. In unloading from point A_{rough} , it is clear that pull-off will occur quite soon in C_{rough} , although for a much larger tensile stress than in the smooth case. The behaviour of the system is however generally well represented by the two envelope curves, corresponding to $\alpha_{d,rough}^{loading}, \alpha_{d,rough}^{unloading}$ respectively for loading and unloading, on which we will build some results in the next paragraph, except for the details of what happens near zero crack size.

The cases in Fig.3b,c are for $\hat{p}^* = 3, 5$ and show an increasing effect of roughness. We have that the equilibrium point A can correspond to crack sizes larger than the point of maximum pull-off, so that the effective pull-off is smaller than the highest point, although still larger than the smooth case. We shall return on these important elements when we will compute the pull-off value as a function of the system parameters (loading and geometrical ones). Also, for the case (c) we have that the jump into full contact, due to increased roughness, moves increasingly towards very small crack sizes, and much higher values of compression, higher than in the smooth case. In this case, also the envelope solution breaks down, since the crack size becomes comparable to the wavelength of the sinusoidal roughness, and hence while the envelope solution suggests full contact only at infinite compression and zero crack, the actual system will show a true jump into contact depending on the full solution.

Naturally, this behaviour also results in an increased hysteresis, since when we follow some loading/unloading cycles (particularly from high pressures even if not enough to jump into full contact), with all the unstable

jumps which dissipate energy in the form of elastic waves emitted in the surface, and this can result in an higher dissipation than in the smooth dimple case. To compute this with precision, one should integrate load-displacement curves.

3.1. Using envelope curves alone

If we make the approximation that the wavelength is very small with respect to the dimple size, the envelope curves joining all maxima and minima of the true solution are a good approximation, and permit a very simple analysis of the behaviour: the effect of roughness corresponds to split the loading and unloading curves into two curves for smooth dimples at different α_d . For example, Fig.4 shows the envelope loading and unloading curves for a case with $\alpha_d = 1$ which, in the smooth case, is unstable whereas in the rough case, for $\alpha = 0.5, 1$ as in the figure, has an equilibrium point: this corresponds to a crack size \hat{c} which becomes very large for low α , and at the same time the unloading curve becomes very high (corresponding to a value which would not be of interest for a smooth dimple, since it would be in that case all unstable). In other words, the system shows that full contact becomes remote, and viceversa, one has a very pressure-sensitive behaviour, as the highest pull-off becomes achievable only for large enough preliminary pre-load.

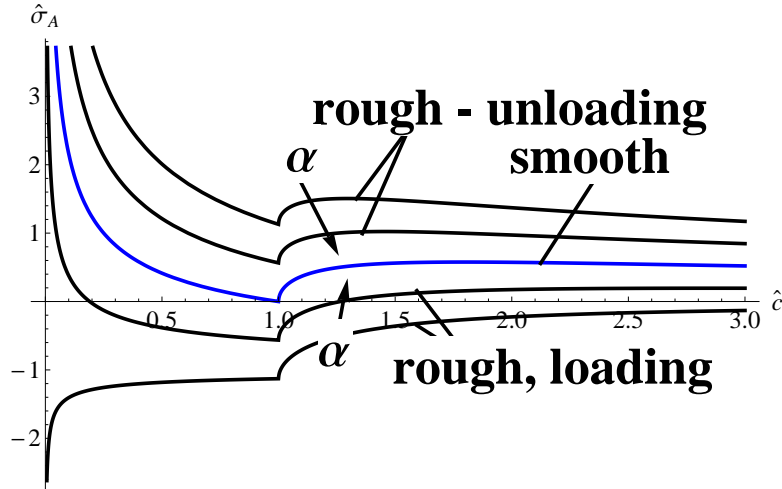


Fig.4. Equilibrium curves for smooth dimple with $\alpha_d = 1$ (blue solid line), together with envelope curves for rough dimple with $\alpha = 0.5, 1$ on loading and unloading.

An aspect which is different from the Guduru-Kesari problem is that we have shown how the effect of roughness tends to put some barrier to the jump into full contact. We can assume that the condition of jump-into-full-contact remains $\hat{c} = 1$: strictly this requires that $\alpha > \frac{1}{\sqrt{\pi}} = 0.56$, but since after that the system is not governed by the envelope solution, we shall make this approximation and therefore estimate

$$\hat{\sigma}_A^{FC} \simeq -1 + \alpha_{d,rough}^{loading} = -1 + \alpha_d \left(1 - \frac{1}{\sqrt{\pi}\alpha} \right) \quad (23)$$

This is shown in Fig.5, where it is clear that we need to push as hard as in the adhesionless condition, if $\alpha = 0.56$; on the other hand, that a partial contact state is found for a much wider range of conditions than in the smooth case, and namely for $\hat{\sigma}_A^{FC} < 0$ which occurs for

$$\alpha_d < \frac{1}{1 - \frac{1}{\sqrt{\pi}\alpha}} \text{ or } \alpha > \frac{1}{\sqrt{\pi}} = 0.56 \quad (24)$$

instead of $\alpha_d < 1$ of the smooth case.

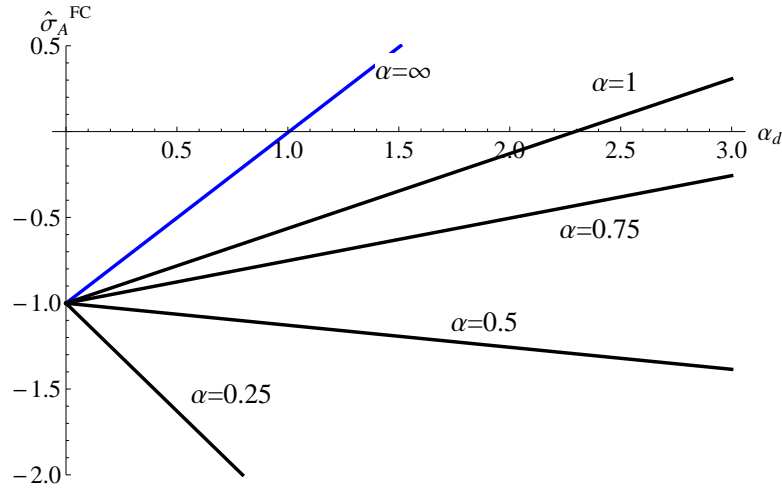


Fig.5. Tension to jump into full-contact $\hat{\sigma}_A^{FC}$ as a function of parameter $\alpha_d = 1$ for various roughness parameter $\alpha = 0.25, 0.5, 0.75, 1, \infty$. The case $\alpha = \infty$ (blue solid line) corresponds to the smooth dimple, whereas for the cases of small $\alpha < 0.57$ we have taken an upper bound estimate considering the value reached at $\hat{c} = 1$, as otherwise the actual minimum depends on the details of the system, see also "Discussion".

3.2. Upper bound to pull-off

Moving to some consideration of pull-off, for the unloading curve from a partial contact condition, we know the size of the contact for pull-off from the solution of the smooth geometry (McMeeking *et al.* 2010), which however should now be computed for $\alpha_{d,rough}^{unloading}$. The full expression is

$$\widehat{c}_{\max} = (m + n)^{1/3} + (m - n)^{1/3} \quad (25)$$

where $m = \frac{2}{(\alpha_{d,rough}^{unloading})^2}$, and $n = \sqrt{m^2 - \frac{1}{27}}$, but this result can be fitted very well with

$$\widehat{c}_{\max} \simeq 1.82 / \left(\alpha_{d,rough}^{unloading} \right)^{0.65} \quad (26)$$

A good expression for $\widehat{\sigma}_{A,smooth}^{PO}$ then turns out to be ($\alpha_d < 1$ is the limit to have a partial contact state in the smooth surface case)

$$\widehat{\sigma}_{A,smooth}^{PO} \simeq 0.53 \alpha_d^{1.3} < 0.53 \quad (27)$$

Therefore, an upper bound to the pull-off for the rough case (where upper bound means provided we have sufficient pre-load as to reach this stage) is

$$\widehat{\sigma}_{A,rough}^{PO \max} = 0.53 \left(\alpha_{d,rough}^{unloading} \right)^{1.3} = 0.53 \left(\alpha_d \left(1 + \frac{1}{\sqrt{\pi\alpha}} \right) \right)^{1.3} \quad (28)$$

and hence the enhancement is really defined by the ratio

$$\frac{\widehat{\sigma}_{A,rough}^{PO \max}}{\widehat{\sigma}_{A,smooth}^{PO}} = \left(1 + \frac{1}{\sqrt{\pi\alpha}} \right)^{1.3} \quad (29)$$

but this time the expression holds as long as we satisfy the condition for partial contact (24). In Fig.6a, we plot for representative cases the value of $\widehat{\sigma}_{A,rough}^{PO \max}$ together with $\widehat{\sigma}_{A,smooth}^{PO}$ (which corresponds to $\alpha = \infty$ and is plotted with blue solid line). As it is clear, already for $\alpha = 1$ we have a significant increase (about 77%), but this holds only until we have the possibility of partial contact solution (this is indicated with arrows going upwards indicating the regime of full contact and "strong adhesion"). However, it is with $\alpha < 0.57$ that the increase becomes really substantial and in principle without limit (see the Discussion paragraph). Supposing we can apply the solution for $\alpha = 0.25$, this corresponds to an enhancement of a factor 4.6.

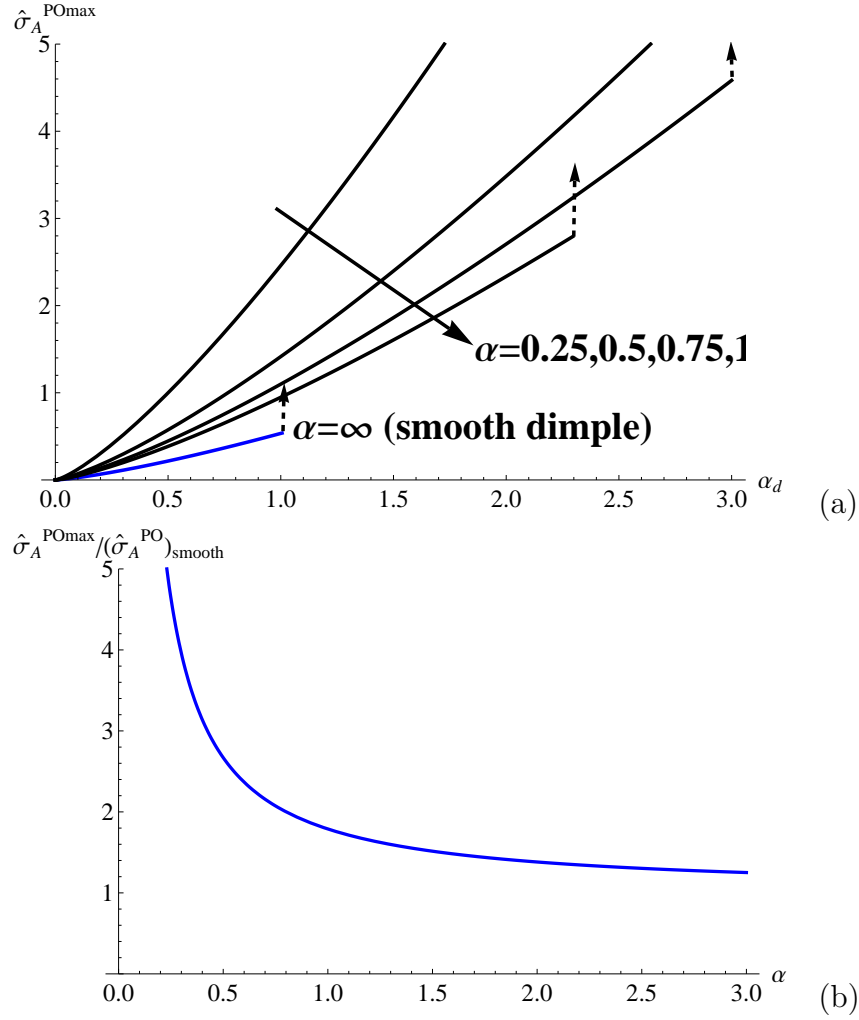


Fig.6. (a) Pull-off $\hat{\sigma}_A^{POmax}$ for rough dimple as a function of α_d for various $\alpha = 0.75, 1, \infty$ (smooth dimple). (b) enhancement factor $\frac{\hat{\sigma}_A^{POmax}}{\hat{\sigma}_A^{PO,smooth}}$ as a function of α

3.3. Pressure-sensitive pull-off

It is clear that, in the case of the smooth dimple, the equilibrium size of the crack at zero load \hat{c}_{eq} is always smaller than the size at pull-off, \hat{c}_{max} . Unfortunately, the expression for \hat{c}_{eq} for the smooth dimple is a little lengthy

$$\hat{c}_{eq} = \frac{1}{12\alpha_d^2} \left[\alpha_d^4 + \frac{\alpha_d^{8/3} (24 + \alpha_d^4)}{p} + \alpha_d^{4/3} p \right] \quad (30)$$

where $p = \left[36\alpha_d^4 + \alpha_d^8 + 24 \left(9 + \sqrt{3} \sqrt{27 + \alpha_d^4} \right) \right]^{1/3}$. It can be approximated by $\hat{c}_{eq} = 0.7/\alpha_d^{0.65}$ but only up to $\alpha_d < 0.4$.

Now, for small roughness, i.e. large α , the loading curve will be close to the loading curve of the smooth case, and therefore the equilibrium crack size $\hat{c}_{eq} \left(\alpha_{d,rough}^{loading} \right)$ will be increased only marginally, while the unloading curve will have moved the point of pull-off to smaller sizes $\hat{c}_{max} \left(\alpha_{d,rough}^{unloading} \right)$. Using the power law approximations for \hat{c}_{eq} and \hat{c}_{max} , we obtain the coincidence and pull-off is unique for

$$\alpha > \alpha_{uni} \simeq 0.9 \quad (31)$$

A more exact calculation shows that α_{uni} varies by only few percent depending on α_d . Therefore, there is an interesting range below α_{uni} which show pressure-sensitiveness. We shall now investigate a little more this range.

For the pressure-sensitive pull-off range, $\alpha < \alpha_{uni}$, a simple but good approximation (provided the wavelength of the roughness is short enough) is that we load up to a certain $\hat{\sigma}_A$, and since we end up in the unloading unstable branch, we will have immediately pull-off. Hence, loading up to

$$\hat{\sigma}_{A,peak} = -1 + \sqrt{1 - \frac{1}{\hat{c}_{peak}^2}} + \frac{\alpha_{d,rough}^{loading}}{\sqrt{\hat{c}_{peak}}} \quad (32)$$

results in a pull off

$$\hat{\sigma}_A^{PO} = -1 + \sqrt{1 - \frac{1}{\hat{c}_{peak}^2}} + \frac{\alpha_{d,rough}^{unloading}}{\sqrt{\hat{c}_{peak}}} \quad (33)$$

We need, in fact, to explore only the range

$$\hat{c}_{max} \left(\alpha_{d,rough}^{unloading} \right) < \hat{c}_{peak} < \hat{c}_{eq} \left(\alpha_{d,rough}^{loading} \right) \quad (34)$$

as otherwise, the upper bound pull-off is obtained, which we have already estimated.

A set of results is shown in Fig.7. It is shown that the pull-off pressure grows at first *linearly with preload*, and then saturates to a value which we have already estimated in (28) and Fig.6. If we continue the curves above this value there would be a second transition towards full contact, which however we did not include in the Figure, for simplicity. In Fig7a,b,c, the case

of $\alpha_d = 0.5, 1, 1.5$ respectively are represented, and an horizontal gray line indicates the pull-off value for the smooth dimple. This permits to estimate the enhancement whose maximum value corresponds to the scale in Fig.6. For larger values of α , the maximum enhancement is smaller, however the sensitivity to the pre-load is higher, so it is possible to have higher pull-off, for a given preload.

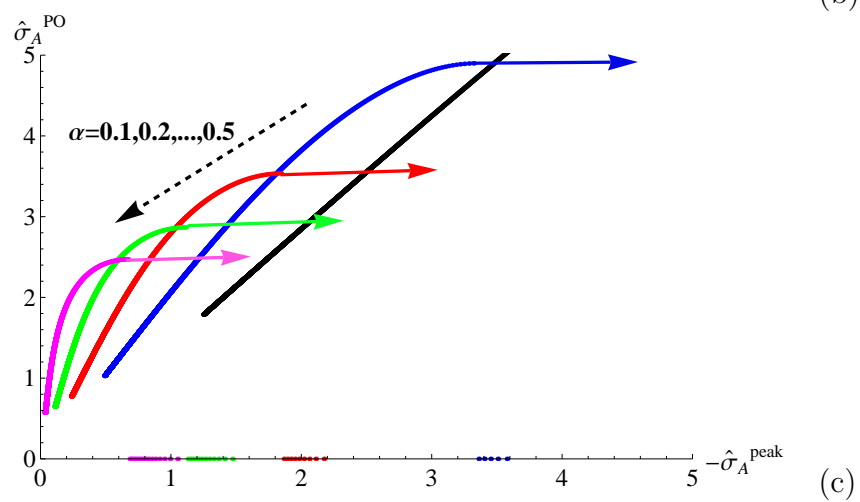
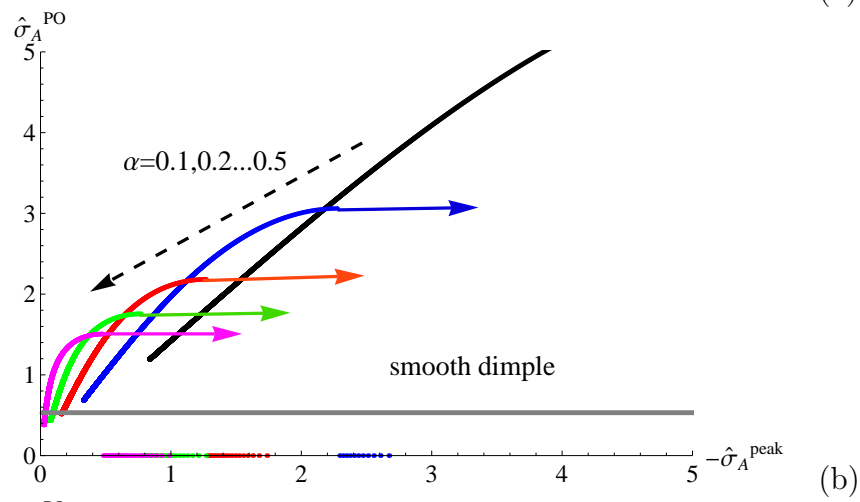
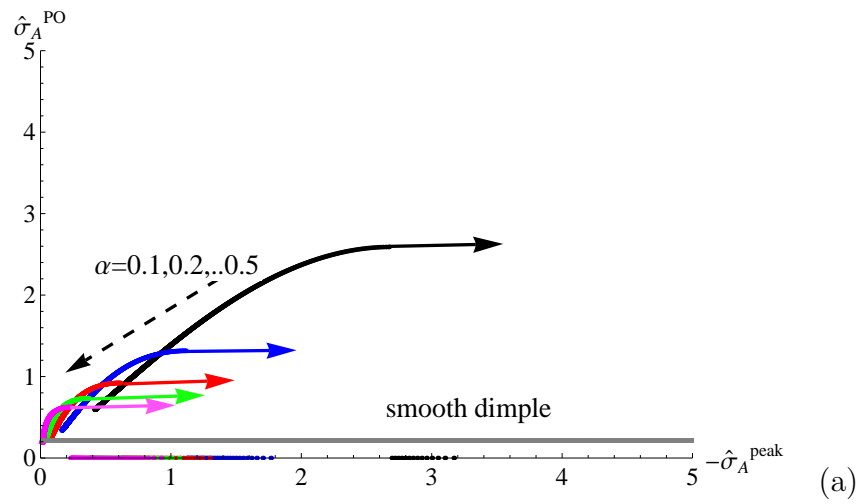


Fig.7. Pressure-sensitive pull-off $\hat{\sigma}_A^{PO}$ as a function of preload $-\hat{\sigma}_{A,peak}$ for three cases of $\alpha_d = 0.5, 1, 1.5$ (a,b,c, respectively)

4. Discussion

Regarding the validity of the solution, some of the conclusions reached in Guduru (2007), but also Ciavarella (2016a, 2016b) translate into this problem, and viceversa, the present solution clarifies some limitations of the Guduru solution. In other words, we are assuming from the outset that a continuous single connected (non-contact) area is obtained. When roughness is very large, as is the case when α is low, we can imagine that this is not the way the solution proceeds. Indeed, contact could be established only in the crests and proceed from crest to crest, before a continuous contact is possible. This explains why, *counterintuitively*, we have reached the conclusion that unbounded enhancement occurs for conditions of large roughness i.e. when Johnson parameter is very low. Guduru’s geometry (the sphere, in fact approximated as a paraboloid) is such that one could postulate that any enhancement should occur after sufficiently large pressure has been applied — although this at one point would involve finite strains in the sphere. In Guduru’s problem, $\alpha = 0.57$ corresponds to an enhancement of the sphere pull-off of a factor 4 — see Ciavarella (2016a), whereas in our dimple case, from (28) we have a value which is slightly smaller, $2^{1.3} = 2.46$ for $\alpha = 0.57$. However, Guduru & Bull (2007) have actually demonstrated values of enhancement higher than 15 in experiments and there is no reason not to expect similar order of magnitude also in our dimple case, justifying our figures above which contain also the case $\alpha = 0.1$. More precise estimates about this limit are not obvious: as Guduru (2007) remarked the limit is not the monotonicity of the profile. Another limit to the enhancement is that our analysis is limited to the JKR regime of large soft materials with high adhesion.

We have not discussed in great details the detachment from full contact. Johnson (1995) also does not discuss in detail for his sinusoidal waviness case, referring to the fact that we need a tension of the order of theoretical strength, and suggests air entrapment, contaminants, or indeed finer scale roughness, may reduce this. In fact, even for a single scale of waviness, a Maugis solution (Hui *et al*, 2001, Jin *et al*, 2016a, Jin *et al*, 2016b) shows that detachment will start when the *peak stress in the full contact state* reaches the theoretical strength, and in our case this means

$$\hat{\sigma}_A = \hat{\sigma}_0 - 1 - \hat{p}^* \tag{35}$$

although the actual critical condition to open the contact will depend also on the COD (Crack Opening Displacement) which has to reach the Maugis range of attraction forces. However, this shows that when the sum of $T + p^*$ is comparable to the theoretical strength, we can start opening already at values much smaller than theoretical strength. This limit is not so remote, since it occurs when the height of the dimple compared to its width (and/or the amplitude of waviness compared to the wavelength), become of the order of 0.1. Indeed, as theoretical strength is of the order of $\sigma_0 \simeq 0.05E^*$, even for $g/\lambda = 0.1$ we have $p^* = 0.3E^* = 6\sigma_0$.

In the presence of roughness and the shallow depression, the "strong adhesion" regime due to full contact disappears in realistic cases, and it will depend also on some appropriate Tabor parameter. Also the enhancement of the "weak adhesion" regime will depend on appropriate Tabor parameter, but a full solution to the problem requires a full numerical investigation, outside the scopes of the present paper.

5. Conclusions

Originally, McMeeking *et al.* (2010) introduced the "dimple" model as a simple geometrical model to explain a bistable system realized with just elastic materials and van der Waals adhesive forces, showing the possible switch from "strong adhesion" realized when pushing in full contact from the stable intermediate equilibrium, to "weak adhesion", when this pressure is not impressed, and one has the pull-off from the partial contact state. The analysis we conducted shows that, with roughness, the dimple model shows a much higher resistance to jump into full contact, and therefore the "strong adhesion" is obviously an ideal limit on two grounds: first, it may be difficult to achieve due to geometrical imperfections, depressions, air entrapment, contaminants, and roughness indeed; second, the separation from this state may not be as difficult as expected, for the same very reasons. However, we showed that, partially balancing this effect, we have an "enhancement" of the "weak-adhesion" regime, which may serve the purpose if one can calibrate the geometry. We have shown a reduced parametric dependence of the system in the asymptotic expansion for small wavelength roughness on only two dimensionless parameters, one being the Johnson parameter for the sinusoid, and the other the corresponding Johnson parameter for the dimple. We obtained that when roughness is relatively large, a pressure-sensitive region is expected, and in this region, the actual pull-off depends monotonically on

the pre-load, and indeed in a significant regions of parameters, linearly on pre-load. The model adds to our understanding of the effect of multiscale roughness on adhesion, which remains a complex problem in the general case.

6. Acknowledgements

A.P. is thankful to the DFG (German Research Foundation) for funding the project HO 3852/11-1.

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8. Appendix. On the use of plane strain approximation.

In (4), we used a plane strain approximation, under the assumption that except perhaps for the first 2-3 oscillations, the problem really is plane strain. However, here is a numerical proof. Obviously we meant (4) for a sinusoidal wave roughness of amplitude g and wavelength λ ,

$$f(r) = g \left(1 - \cos \left(\frac{2\pi r}{\lambda} \right) \right) \quad (36)$$

If we take the standard cumulative superposition approach used by Guduru (2007) and take the contact area $c \rightarrow \infty$, we get

$$h(c) = c \int_0^c \frac{f'(x) dx}{\sqrt{a^2 - x^2}} = \pi^2 \frac{g}{\lambda} c H_0 \left(\frac{2\pi c}{\lambda} \right) \simeq -\pi \sqrt{\frac{c}{\lambda}} g \sin \left(\frac{\pi}{4} - \frac{2\pi c}{\lambda} \right) \quad (37)$$

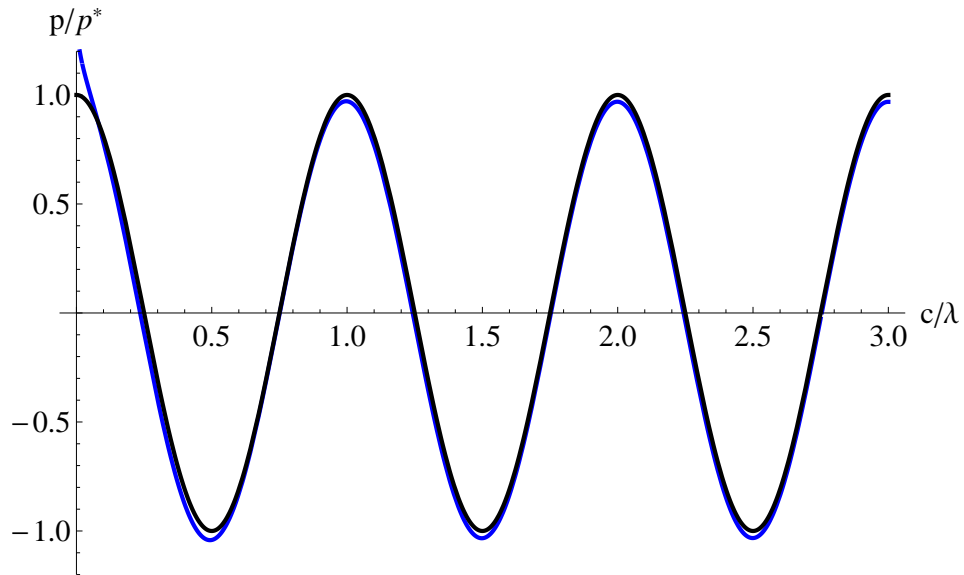
which we have expanded for small λ . Taking only the leading term in the derivative $h'(x)$ and using

$$p(r) = \frac{E^*}{\pi} \int_r^c \frac{h'(x) dx}{\sqrt{x^2 - r^2}} \quad (38)$$

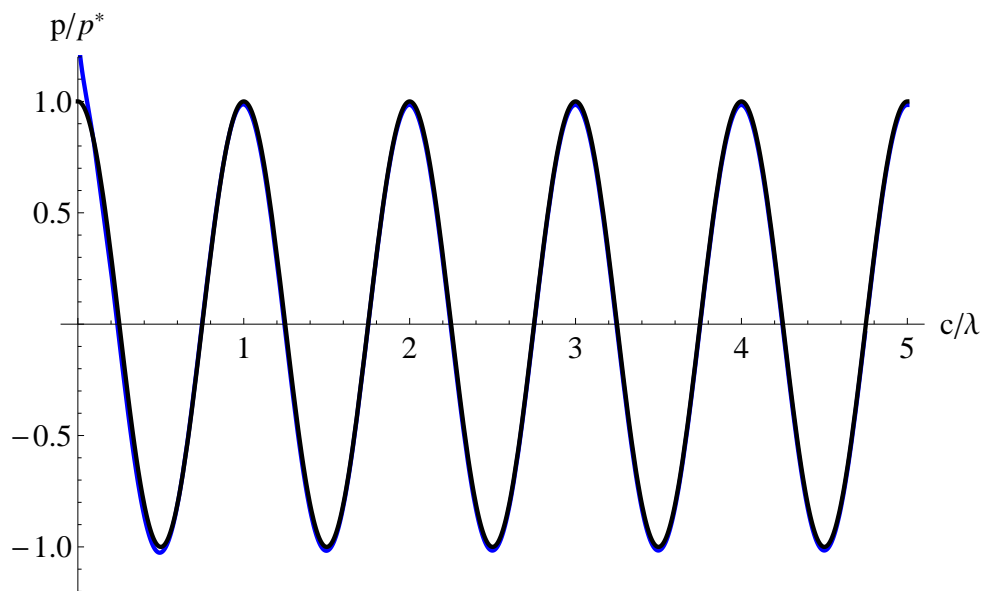
we find that

$$\frac{p(r)}{p^*} = 2\sqrt{\frac{c}{\lambda}} \int_r^c \frac{\cos\left(\frac{\pi}{4} - \frac{2\pi x}{\lambda}\right) dx}{\sqrt{x^2 - r^2}} \quad (39)$$

When we take $c = 50\lambda$ (Fig.A1a) we find that the error is negligible but perhaps still visible on the first oscillations, but this reduces further with $c = 100\lambda$ (see Fig.A1b), and as we are considering here the full contact pressure when $c = \infty$, we do not need to worry about this approximation.



(a)

As Fig.1, but for $c = 100\lambda$.

(b)

Fig. A1 Function $\frac{p(r)}{p^*}$ numerically obtained (blue solid line) for $c = 50\lambda$, against the plane strain solution $\cos(2\pi c/\lambda)$. (solid line). (b) but for

$$c = 100\lambda.$$