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Heavy metals retention (Pb(II), Cd(II), Ni(II)) from single and multimetal solutions by natural biosorbents from the olive oil milling operations

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1	Heavy metals retention (Pb(II), Cd(II), Ni(II)) from single and multimetal
2	solutions by natural biosorbents from the olive oil milling operations
3	
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17	
18	Abstract. In the present paper, the lignocellulosic residues from the olive oil industry in South-East
19	Italy, namely BOP (Biosorbent from Oil Production), were used as sorbents for heavy metals
20	retention (Pb <sup>+2</sup> , Cd <sup>+2</sup> , Ni <sup>+2</sup> ) in water and wastewater treatments.
21	To the purpose, thermodynamic and kinetic investigations for single and multispecies systems were
22	carried-out through batch equilibrium isotherms and column dynamic experiments.
23	In the case of batch tests, maximum metals retentions $(q_{max})$ in single ion solutions were 22.4
24	mg/g <sub>BOP</sub> , 10.5 mg/g <sub>BOP</sub> , 5.04 mg/g <sub>BOP</sub> respectively for Pb <sup>+2</sup> , Cd <sup>+2</sup> and Ni <sup>+2</sup> , lower figures were
25	detected in the case of ternary systems with values exceeding 10.51 mg/gBOP, 5.11 mg/gBOP, 3.81

 $mg/g_{BOP}$  respectively. Further drastic reductions were detected in tap water. Langmuir and Freundlich isotherms led to good correlations of the data in single-ion and ternary solutions in demineralized water. Freundlich isotherms gave better correlation in tap water.

29 In the case of column tests, operating capacities resulted in the same order with  $Pb^{+2} > Cd^{+2} > Ni^{+2}$ .

30 After retention, the exhausted metal converted materials were included into cement conglomerates 31 for a possible employment in the building industry applications, thus minimizing their potential 32 environmental impact.

33

34 Keywords: Olive waste; Sorption; Porous media; Batch reactor; Column dynamic experiment;
35 Wastewater treatment

36

# 37 **1.Introduction**

38 Biosorption relies on the use of natural residues from the agro-food industry to remove organic and 39 inorganic pollutants present in wastewater of different nature and origin (Abdolali et al., 2014; 40 Ahmad et al., 2017; Ashraf et al., 2017; Cifci, and Meric, 2016; Fomina and Gadd, 2014; Ismail et 41 al., 2017; Jafar Ahamed et al., 2017; Kahn et al., 2017; Michalak et al., 2013). Among vegetal waste 42 materials, husks from: a) the olive oil milling operations (Doyurum and Celik; 2006; El-Kady et al.; 43 2016; Ronda et al., 2016); b) wheat and maize crops (Mosa et al., 2016; Qi et al., 2016); c) plant 44 root tissues (Chiarantini et al., 2016; Rezania et al., 2016); d) fruit residues (Ahmad et al., 2016; do 45 Nascimento et al., 2016) are widespread in all the Mediterranean areas. Above wastes result to be 46 particularly versatile toward removal of biopersistent pollutants from wastewater due to their low 47 cost (if any), ready availability and eco-compatibility at large, thus representing a valuable 48 alternative to conventional sorption technologies from both technical and economic points of view 49 (do Nascimento et al., 2016; Qi et al., 2016; Rezania et al., 2016). Other advantages are associated 50 with their high efficiency, already at very low concentrations ( $\mu$ g/L), no production of toxic sludge

after conventional precipitation and, above all, the possibility of recovery energy and valuable
materials after burning down of the exhausted sorbents (Chouchene et al., 2014; Fernández-Pereira
et al., 2011).

54 In the present paper, the retention (sorption) of biopersistent pollutants from industrial wastewater 55 was obtained by the use of biosorbents from the olive oil milling operations (pressing and chemical 56 extraction), namely BOP (Biosorbent from Oil Production), deriving from the South-East Italy. 57 Specifically, BOP residues include partially decomposed lignocellulosic materials from peel and 58 olives kernel. The solid fraction is characterized by a carbohydrate (cellulosic) backbone including 59 carboxylic and phenolic functional groups (Baccar et al., 2009; Chao and Chang, 2012; 60 Konstantinou et al., 2007; Martín-Lara et al., 2009). Due to the substantially high transport and 61 disposal costs of these wastes, the high water content which does not allow for their direct 62 landfilling and the low revenues from the olive oil production, reuse of the reference materials is 63 almost imperative for best economic management of the waste. Specifically, 75% of the annual 64 worldwide production of olive oil comes from European Union countries around the Mediterranean Sea (average olive harvest of 10<sup>7</sup> tons per year). Considering that the demand of olive oil is rapidly 65 66 increasing, environmental pollution due to olive mill liquid and solid wastes is a growing problem 67 especially in the Mediterranean region. In fact, after the processing of 1 ton of olive, 200 kg of oil 68 are produced with 600-1200 kg of wastewater and 400-600 kg of solid wastes characterized by a 69 water content ranging between 25% and 50% (Azbar et al., 2004). For these reasons, the objective 70 of this paper was to use this local BOP as secondary raw material in wastewater treatments, 71 specifically for the retention of biopersistent pollutants as heavy metals. The present idea may 72 represent a convenient, original and valid alternative in the environmental control operations, 73 because a non-conventional sorbent may be also used for the removal of such toxic compounds as 74 lead, cadmium and nichel ions. In fact, an incremental release of heavy metals in the environment 75 has been the consequence of the increasing industrial use over the past decades (Femina Carolin et 76 al., 2017, Azimi et al., 2017, Fu and Wang, 2011, Zhao et al., 2016, Shanmugam and Arabi

Mohammed Saleh, 2016). Leather tanning, mining and metal plating industries are among the main sources of e.g. lead, cadmium, copper, chromium, arsenic, zinc and nickel ions. Industrial effluents containing heavy metals represent a serious environmental problem due to the essential biopersistence of these pollutants leading to unacceptable sanitary risk and hazards in all natural compartments including man (Bánfalvi, 2011; Satyro et al., 2014).

In the present work, the retention properties of the BOP cellulosic biosorbent were evaluated in batch (equilibrium) and column (dynamic) tests. The Langmuir and Freundlich isotherms were used to correlate equilibrium data (Freundlich, 1906; Langmuir, 1918). Specifically, the sorbents were assumed to be used *"in once through operations"* to minimize problems related with the regeneration step, i.e., costs of regeneration chemicals, end disposal and fate of the hazardous spent regeneration eluates, etc.

After exhaustion, metals laden residues could be considered toxic, but the final aim of this paper was to propose the possible re-use the reference polluted secondary raw materials for applications in the building industry, specifically in lightweight cement conglomerates formula thus minimizing their potential impact to the environment (Petrella et al., 2016, 2012).

92 So, in summary, the objective of this study relies in the application of biosorbents from the agro-93 food industry for the removal of heavy metals from water and wastewater, with the final 94 employment of the exhausted lignocellulosic material in the construction field.

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#### 96 **2.Experimental section**

# 97 **2.1 BOP characterization**

BOP for thermodynamic and kinetic tests was acquired from Rubino olive-oil manufacturing, Bari,Italy.

2 kg representative raw sample was initially dried and crushed, then sieved and pre-conditionedwith 1 M HCl and 1 M NaOH solutions (three times) and thoroughly washed with demi water to

102 neutral pH. For practical problems in technological applications in the environmental area (i.e., 103 removal of metals and release of noxious organics to the liquid-phase), it was necessary to clean-up 104 BOP in such a way due to the presence of soluble organics (e.g., fulvic, humic acids, or other 105 degradation products from natural degradation of the cellulosic backbone of BOP). The sorbent 106 was successively air dried and finally put in the oven at 105°C. The dried material was crushed 107 again in the range 1-3 mm before testing.

108 Elemental analysis was performed with Euro EA Elemental Analyser, Wegberg, Germany, the 109 average BOP composition was 47% C, 2.7% N, 5.5% H, 44.8 O (Jain et al., 2013).

SEM morphology confirmed that BOP surface exhibits a linear groove structure with regular porous and fine fibers (Fig. 1). The samples were fixed on aluminium stubs with colloidal graphite and then sputtered with a 30 nm thick carbon film using an Edwards Auto 306 thermal evaporator. Backscattered electron (BSE) images were obtained with a Zeiss scanning electron microscope (SEM) model EVO50XVP (Carl Zeiss Microscopy GmbH, Jena, Germany). SEM operating conditions: accelerating potential 15 kV; probe current 500 pA.

EDX analysis of metals laden BOP was obtained by an electron microscope FESEM-EDX Carl
Zeiss Sigma 300 VP (Carl Zeiss Microscopy GmbH, Jena, Germany).

BET surface area and pore size of the sorbent were determined by adsorption-desorption N<sub>2</sub> isotherms at 77 K, by an Autosorb IQ Chemi TCD instrument (Quantachrome Instruments, Boynton Beach, FL, USA). The biosorbent was apparently a mesoporous material with pore diameters ranging 20-500 Å, average pore radius 15.649 Å and BET total surface area exceeding  $0.324 \text{ m}^2/\text{g}$ . Referring to the pores, the total volume and surface area were respectively  $0.002 \text{ cm}^3/\text{g}$  and  $0.225 \text{ m}^2/\text{g}$ .

- 124
- Figure 1.
- 126

FTIR-ATR spectra of BOP (Fig. 2A) was recorded within the 600–4000cm<sup>-1</sup> range using a Fourier 127 128 Transform Infrared spectrometer 670-IR (Agilent Technologies Inc., Santa Clara, CA, USA), whose 129 resolution was set to 4 cm<sup>-1</sup>. Specifically, 32 scans were summed for each acquisition. The surface incidence of the main functional groups of BOP was clearly observed, under the experimental 130 131 conditions (Akar et al., 2009). Bands were detected in the wavenumber region between 3600 and 2800 cm<sup>-1</sup> and 800-1800 cm<sup>-1</sup>. The vibration detected at 3313 cm<sup>-1</sup> suggested the presence of 132 hydroxyl and amino moieties (Mousa et al., 2009). The former could be ascribed to cellulose and 133 hemicellulose molecules, better evidenced at 1032 cm<sup>-1</sup> and 1162 cm<sup>-1</sup>, the latter to amino acids 134 135 and/or proteins (Rizzi et al., 2017). The incidence of amino and carboxyl groups was inferred observing the bands at 1540 cm<sup>-1</sup> and 1630 cm<sup>-1</sup>. As for the presence of phenols and polyphenols, 136 137 vibration modes of CH<sub>3</sub>, CH<sub>2</sub>, C-H moieties along with the stretching of polyphenolic aromatic rings C-C were detected between 1100 and 1500 cm<sup>-1</sup> (Omar and Abd El -Baset Attia, 2013). Not 138 surprisingly, the presence of lignin was confirmed observing the bands at 2920 cm<sup>-1</sup> and 2840 cm<sup>-1</sup>, 139 140 assigned to C-H stretching of methyl and methylene groups. Others signals were detected at 1318 cm<sup>-1</sup> and 1241 cm<sup>-1</sup> indicating the C-O vibrations of carboxylate groups and the stretching of esters, 141 142 ethers or phenol groups (Paganelli et al., 2003).

TGA were performed using STA 449 F1 Jupiter, Netzsch, Selb, Germany. The sample was
analyzed in the range 25-550°C at the heating speed of 3°C/min and in air atmosphere.

145 TG and DTG analyses were performed in order to unveil the FTIR-ATR findings. Results are 146 reported in Figure 2B. The typical curve of solid fuels, having several weight losses, was obtained. 147 As expected, as a first step the evaporation of the free moisture content was observed at around 100 °C followed by important weight losses in the temperature range between 200 to 400 °C and 410-148 149 500 °C. The temperatures of decomposition suggested the presence of hemicellulose, cellulose and 150 lignin. Indeed, in excellent agreement with literature (Kabakci and Aydemir, 2013, Tawarah and Rababah, 2013, La Rubia Garcia et al., 2012) the hemicellulose/cellulose degradation occurs 151 between 200 and 350 °C with maximum rate of degradation at 269°C as observed in the present 152

condition (if the hemicellulose degradation was exactly at 269°C, the cellulose decomposition
occured at above 320 °C); the decomposition of lignin also occurs in this range of temperature and
continued up to 600 °C (see inset Figure 2B, the peak at 333 °C).

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- 157

#### Figure 2.

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### 159 2.2 Sorption experiments. Batch (equilibrium) and column (dynamic) tests

Sorption experiments were carried out by the use of 1-3 mm BOP samples which were contacted
with metals containing solutions representative of typical industrial wastewater. Synthetic solutions
were prepared from reactive grade Pb(NO<sub>3</sub>)<sub>2</sub>, Cd(NO<sub>3</sub>)<sub>2</sub>•4H<sub>2</sub>O, Ni(NO<sub>3</sub>)<sub>2</sub>•7H<sub>2</sub>O from Carlo Erba,
Milan, Italy.

Batch equilibrium isotherms were correlated by Freundlich and Langmuir models. Application of Langmuir and Freundlich models is strictly dependent from the nature of the equilibrium data (Freundlich, 1906; Langmuir, 1918). The first model is conventionally applied for monolayer sorption when all the adsorption sites are equivalent and able to accommodate only one molecule:

$$168 \qquad q_{eq} = \frac{q_{max}bC_{eq}}{1+bC_{eq}} \tag{1}$$

169  $q_{eq}$  is the observed retention capacity onto the sorbent (mg/g);  $q_{max}$  is the maximum retention 170 capacity (mg/g); *b* is an equilibrium constant;  $C_{eq}$  is the equilibrium concentration (mg/L).

171 Langmuir equation may be linearized to get the sorption constants:

172 
$$\frac{C_{eq}}{q_{eq}} = \frac{1}{q_{max}b} + \frac{C_{eq}}{q_{max}}$$
(2)

173 Freundlich model, represented by the following empirical equation, assumes heterogenous surface:

$$174 \quad q_{eq} = K_f C_{eq}^{1/n} \tag{3}$$

175  $K_f$  is a constant related to the sorption capacity; *n* is related to the sorption intensity (energy) at the 176 functional groups;  $C_{eq}$  is the equilibrium concentration (mg/L). 177 The Freundlich equation too may be rearranged to the linear form to get the relative constants:

$$178 \quad lnq_{eq} = \frac{1}{n} lnC_{eq} + lnK_f$$

From the applicative point of view, in a first set of batch experiments, single metal containing solutions in demi-water (200 cm<sup>3</sup>, 10 mgMe<sup>+2</sup>/L, pH = 6) were contacted with known amounts of sorbent in the range of 2–400 mg. In a second set of batch experiments, ternary metal solutions in demi-water (200 cm<sup>3</sup>, 10 mg Me<sup>+2</sup>/L each, pH = 6) were contacted with the sorbent in the range of 5–600 mg. In a third set of batch experiments, ternary metal containing solutions in tap-water (200 cm<sup>3</sup>, 0.3 mg Me<sup>+2</sup>/L each, pH = 7.5) were contacted with the sorbent in the range of 1–100 mg.

Equilibrations were carried-out in vials at 25°C by the use of a rotating stirrer (80 rpm) for one day, i.e., when the supernatant solution concentration changed by less than 5% after two subsequent samplings.

Laboratory column (dynamic) tests allowed for a deeper insight into the interactions of metals at the liquid-solid interface by the construction of the metals breakthrough curves. Breakthrough curves represent the variation of the relative effluent concentration ( $C/C_0$ ) eluted by the column along time (t) or the effluent liquid volumes at constant flow-rate in the column (Bed Volumes, BV). The breakpoint corresponds to the minimum retention capacity of the sorbent toward metals packed into the column. Complete exhaustion of the biosorbent corresponds to equal concentrations of the effluent and influent solutions flowing through the column.

From an applicative point of view, column experiments were carried by the use of jacketed glass column (I.D. = 1.0 cm; H = 50 cm) packed with 5.5 g of BOP. Elution of the column was carried out with demi-water ternary metals solution (10 mg Me<sup>+2</sup>/L each, pH = 6) at a flow-rate ranging 0.7 L/h. Each dynamic test was extended to complete column breakthrough, i.e., when the effluent from the column was equal to the influent solution concentration.

200 Liquid-phase metals concentrations, detected during batch and column experiments, were
201 determined by Flame Atomic Absorption Spectrometry using a Mod. 929 Spectrometer from

Unicam, Milan, Italy. The technique is based on the principle that ground state metals absorb light
at a specific wavelength and metal ions are converted to atomic state by a flame. After absorption of
a specific wavelength, the amount absorbed is measured and a concentration is obtained.
Table 1 summarizes the complex of laboratory tests carried out.

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Table 1.

2.3 Metals leaching test from BOP containing mortars and thermo-mechanical measurements

After exhaustion, heavy metals laden BOP were embedded into cement mortars as replacement of 211 212 the conventional aggregates. Class II CEM A-LL, 42.5R cement, from Buzzi Unicem, Barletta, 213 Italy (Italian Organization for Standardization, 2011), was used to prepare the conglomerates. 400 214 cm<sup>3</sup> BOP was added according to standard protocols (Italian Organization for Standardization, 215 2016), cube samples (4×4×4 cm) were prepared and aged for 28 days at relative humidity, RH 216 >90%, then dried to constant weight. Specimens were submitted to jar test (Vittadini, Aqua, Milan, Italy) to evaluate potential release of Pb<sup>2+</sup>, Cd<sup>2+</sup>, and Ni<sup>2+</sup> species, which was carried out after 217 218 filtration and analysis of the supernatant solution (Italian Organization for Standardization, 2002).

Thermal measurements were carried-out on cylinder specimens ( $\varphi = 100$  mm; H = 50 mm) by a Mod. ISOMET 2104 system, from Applied Precision Ltd (Bratislava, Slovakia), after 28 days curing. Thermal conductivity was determined after placing a heating probe on the front face of the sample thus geerating a constant thermal flow. A normalized mortar was prepared as control.

Mechanical tests (compression) were carried out by a MATEST system, Milan, Italy, on samples deriving from mechanical flexural tests. Specifically, prisms (40×40×160 mm) were prepared according to standard protocols (Italian Organization for Standardization, 2016) and 28 days cured, while normalized mortar was prepared as control.

# 228 **3. Results and discussion**

229 Figure 3A and 3B show batch (equilibrium) curves for single ions metal retention at constant 230 concentration (10 mg/L, 25°C). Freundlich and Langmuir correlations are shown in Figures 3C and 231 3D. Equilibrations were carried-out in de-mineralized water, pH = 6, which was considered the 232 optimum for experimental tests because, as reported elsewhere (Doyurum and Celik, 2006; El-Kady 233 et al., 2016; Fiol et al., 2006; Saeed et al., 2005), sorption for all metals at low pH, i.e., 2-4 was 234 shown to be negligible, with best results in the range of 5-6. Specifically, negatively charged groups 235 at the biosorbent surface are necessary for metals sorption, whereas acidic pH, i.e. 2, limits 236 interactions as a net positive charge on the biosorbent is formed after protonation reaction, thus 237 competing with metals at the active sites. At higher pH, a negatively charged surface is formed onto 238 the biosorbent surface thus favouring metal uptake. Further pH increase induces metals precipitation (Doyurum and Celik, 2006; El-Kady et al., 2016; Fiol et al., 2006; Saeed et al., 2005). 239 240 It was observed that, with the increase of the sorbent dosage, the maximum sorbed quantities  $(mgMe^{2+}/g)$  decreased (Figure 3A) and the metals removal increased (Figure 3B) (Dakiky et al., 241 2002; Pradhan et al., 1999; Rengaraj et al., 2001). Moreover, almost 100% of every metal retention 242 243 was obtained as reported in Figure 3B. Table 2 summarizes the experimental maximum retentions. 244 245 Figure 3.

- 246
- 247

Table 2.

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Maximum retention capacities were determined, for Pb, Cd and Ni respectively, at 22.4; 10.5 and 5.04 mg/g<sub>sorbent</sub>. A relevant role in determining the overall metals retention capacities is played by the BOP specific surface area and the corresponding larger sorbent pores (Figure 1) exposed to the liquid-phase, together with metals hydrated radius. Free migration of metal ions to the functional 253 groups of the biosorbent was allowed by the large openings (porosity) in the cellulosic matrix (Manliu et al., 1994). Accordingly, the free energies of hydration/de-hydration of the metal ions 254 255 should play a more important role in determining the overall interaction onto the biosorbent surface 256 (Robinson and Stokes, 1970). The lowest interaction energy (electrostatic) and hydration radius 257 (hindrance) (Table 3) confirm that lead ions were preferentially sorbed as compared to the largest 258 radius and higher free energy of cadmium ions (Robinson and Stokes, 1970). Indeed, lead ions 259 showed higher retention capacity as compared to cadmium ions because of the most favorable 260 compromise between permeation (smaller hydrated radius) and interaction (easier ionic dehydration 261 at functional groups). Lead ions also showed higher retention capacity as compared to nickel ions; 262 in this case the interaction seems to be preferentially associated with dehydration energy because 263 both ions show almost the same ionic radius. Cadmium ions showed higher retention capacity as compared to nickel ions; in this case electrostatic factors play a more relevant role than steric 264 265 hindrance.

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#### Table 3.

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Moreover, Table 2 shows the relevant models parameters derived from Figures 3C and 3D. Specifically, various direct parameters calculated from the adsorption isotherms, namely, maximum retention capacity ( $q_{max}$ ), adsorption efficiency (b) and confidence parameter ( $R^2$ ) from the Langmuir isotherms, and derived sorption capacity of the sorbent ( $K_f$ ), sorption intensity (1/n) and confidence parameter ( $R^2$ ) from the Freundlich isotherms are shown. The confidence parameters indicate that both models can be applied for data correlation.

Nonetheless, the separation factor  $R_L$  is a characteristic of the Langmuir model and can be calculated from the following equation (Hall et al., 1966):  $R_L = 1/(1+bC_0)$  where  $C_0$  is the initial concentration of the adsorbate (mg/L) and b (L/mg) is the Langmuir constant.  $R_L$  is related to the shape of the isotherm, e.g., unfavorable retention,  $R_L > 1$ ; indifferent equilibrium,  $R_L = 1$ ; favorable equilibrium,  $0 < R_L < 1$ ; irreversible equilibrium,  $R_L = 0$  (Hameed et al., 2009).  $R_L$  values for the metals adsorption on BOP were in the range 0-1, which means favorable retention toward species of interest.

Table 4 shows a comparison with the retention capacities obtained by other authors. Specifically, similar results can be observed in the case of raw materials, although metal sorption figures tend to increase in the case of chemical treatments of the biomass. In the latter case, the modification techniques are employed to enhance and reinforce the functional groups potential and increase the number of active sites.

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#### Table 4.

291 In ternary demi water solutions a definite preference of the biosorbent toward lead ions was also evidenced (Figures 4A and B) (Saeed et al., 2005) with a selectivity scale in the following order: 292  $Pb^{++} > Cd^{++} > Ni^{++}$ . As discussed before (single ion solutions), lead ions showed the best 293 294 performance because of the lowest interaction energy and hydration radius as compared to cadmium and nichel ions. Moreover, at higher sorbent dosage maximum sorbed quantities  $(mgMe^{2+}/g)$ 295 296 decreased (Figure 4A), metals removal increased and almost 100% of every metal retention was 297 obtained (Figure 4B) (Dakiky et al., 2002; Pradhan et al., 1999; Rengaraj et al., 2001). Generally 298 speaking, experimental q<sub>max</sub> exceeding 10.51, 5.11 and 3.81 mg/g<sub>sorbent</sub>, respectively for Pb, Cd and 299 Ni, were observed (Table 5), definitely lower figures as compared to single ion solutions. Reduction 300 in the retention capacities in the case ternary solutions may be attributed to the greater cumulative 301 occupancy by the larger ions at the BOP surface. Freundlich and Langmuir correlations are shown 302 in Figures 4C and 4D, while Table 5 also shows the relevant models parameters. Both models can 303 be applied for data correlation and no significant differences were observed between single and 304 ternary systems. Also in this case the value of  $R_L$  of the Langmuir model indicates a favorable 305 process for the adsorption of the metals on BOP.

306

Figure 4.

Table 5.

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310 In the case of measurements in tap water solutions, the presence of major divalent and monovalent ions, i.e., Ca<sup>2+</sup>, Mg<sup>2+</sup>, Na<sup>+</sup>, etc, determined a large decrease of the retentions (Figures 5A and 5B). 311 Generally speaking, experimental  $q_{max}$  exceeding 1.20, 0.80 and 0.74 mgMe<sup>2+</sup>/g<sub>sorbent</sub>, respectively 312 for Pb<sup>+2</sup>, Cd<sup>+2</sup>, and Ni<sup>+2</sup> were observed (Table 6). On the other hand, potential formation of 313 314 negatively charged metal complexes with anions (chlorides) may lead to Donnan exclusion thus further reducing the biosorbent performance (Helfferich, 1962). Freundlich and Langmuir 315 316 correlations are shown in Figures 5C and 5D, while Table 6 also shows the relevant models 317 parameters.

318 It is known that main peculiarities of the Freundlich and the Langmuir models are the assumption 319 that the first forms a multilayer, the second forms a monolayer of the sorbed species. In this context, 320 experimental data for tests carried-out in demineralized water were pretty well correlated by both 321 models. In the case of the experiments carried-out in tap water, correlations based on the Freundlich 322 model were definitely better than the other. This may be supposedly explained in terms of sorbate multilayer formation. In the case of tap water, the massive presence of alternative ions (calcium and 323 324 magnesium) may preferentially saturate the first layer thus leaving to the minor metal species of 325 interest almost no room for the interaction at the sorbent active groups. This may explain the poor correlation of the Langmuir model. 326

327

329	Table 6						
330	Column (dynamic) tests were carried-out for a deeper insight into the interactions of the metals a						
331	the liquid-solid interface by the construction of the breakthrough curves. Operations were obtained						
332	in stationary conditions by the elution of ternary metals solutions (C= 10 mgMe <sup><math>2+</math></sup> /L each in demi-						
333	water) at constant flow-rate in the column exceeding 0.7 L/h. Fig.6A and B show the experimental						
334	breakthrough curves (Petrella et al., 2012, 2010).						
335							
336	Figure 6.						
337							
338	Relevant data at metals breaktrough are shown in Table 7. Results from the column tests confirmed						
339	thermodynamic data. Also in this case a definite preference of the biosorbent toward lead ions was						
340	evidenced with a selectivity scale in the following order:						
341							
342	$Pb^{++} > Cd^{++} > Ni^{++}$						
343	corresponding to an anticipated breakthrough point in the case of less sorbed metals occurring at						
344	lower effluent Bed Volumes (V/V $_0$ ). The overall operating capacities for different metals, at						
345	complete column breakthrough, resulted to be also in the same order:						
346							
347	$q_{Pb}^{++} > q_{Cd}^{++} > q_{Ni}^{++}$						
348							
349	quantitatively identified in 5.33 mgPb <sup>++</sup> / $g_{BOP}$ ; 2.71 mgCd <sup>++</sup> / $g_{BOP}$ ; and 1.98 mgNi <sup>++</sup> / $g_{BOP}$						
350	respectively, as summarized in Table 7.						
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352	Table 7.						
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From the applicative point of view, in batch (equilibrium) and column (dynamic) operations the sorbents were used *"in once through operations"* to minimize technical and economic problems related with the regeneration step.

For this reason, after retention, metals exhausted materials were finally used (disposed) in cement mortars formula as replacement of conventional aggregates thus minimizing their potential impact to the environment (Petrella et al., 2016, 2012, 2009). To the purpose, in order to evaluate possible release of lead, cadmium and nichel ions, mortar specimens including metals laden biosorbents were submitted to jar test (Italian Organization for Standardization, 2002). It was observed (Table 8) that the release of metals to the liquid-phase was below the maximum allowable concentrations for hazardous waste disposal in controlled landfills.

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# Table 8.

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Moreover, EDX observation for the metal laden BOP showed no particular changes on the structure of the biosorbent and, after semi-quantitative analysis of the heavy metals retained by the solid phase, it was observed that the wt% ratios between the metal species were very comparable with the ratios between the overall capacities (Fig. 7).

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372

# Figure 7.

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After jar test, which demonstrated negligible release of metals, the specimens were characterized for possible applications in the construction field. The preliminary results of the metal laden composites suggest that the specimens show very low thermal conductivities  $\lambda$  (0.18 W/mK) as opposite to the conventional sand based control (2.0 W/mK) but the mechanical properties are quite low (~1 N/mm<sup>2</sup>) which suggests to introduce in the metals laden mortar other metal laden

379	aggregates (recycled porous glass, studied in previous works (Petrella et al., 2012) which can
380	increase compressive resistances.
381	Basically, the application of these conglomerates may be as non structural thermo-insulating and
382	lightweight materials in the construction industry (panels, plasters) due to the presence of a metal
383	laden waste as the lignocellulosic aggregates.
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#### 405 **Conclusions**

The objective of this paper was based on the application of biosorbents from the olive oil milling operations (BOP from South-East Italy) for the removal of lead, cadmium and nichel ions present in water and wastewater, with final possible re-use of the metals laden materials in the construction field.

410 Specifically, the sorption properties of the reference wastes toward metal ions was demonstrated411 through batch (equilibrium) and column (dynamic) tests.

412 In the present case, no preliminary treatments were carried-out on the sorbents to improve the 413 retention capacities.

From batch tests, maximum metals retentions in single ion solutions were 22.4 mg/g<sub>BOP</sub>, 10.5 mg/g<sub>BOP</sub>, 5.04 mg/g<sub>BOP</sub> respectively for Pb<sup>+2</sup>, Cd<sup>+2</sup> and Ni<sup>+2</sup>, while in the case of ternary systems, maximum metals retentions were 10.51 mg/g<sub>BOP</sub>, 5.11 mg/g<sub>BOP</sub>, 3.81 mg/g<sub>BOP</sub> respectively for Pb<sup>+2</sup>, Cd<sup>+2</sup> and Ni<sup>+2</sup>.

418 Best retention toward lead ion was attibuted to the hydrated radius and free energies of 419 hydration/de-hydration of the metal ions.

Reduction in the retention capacities in the case of ternary solutions respect to single ion solutions
may be attributed to the greater cumulative occupancy by the larger ions at the BOP surface.

422 The lowest retentions were detected in tap water due to the presence of major divalent and 423 monovalent ions and to the potential formation of negatively charged metal complexes with anions 424 (chlorides) leading to Donnan exclusion.

425 Langmuir and Freudlich isotherms gave a good correlation of the experimental data in single-ion426 and ternary solutions, while the Freundlich model resulted better in tap-water solutions.

427 Also in the case of the column (dynamic) tests a definite preference of the biosorbent toward lead 428 ions was evidenced with the following retentions: 5.33 mgPb<sup>++</sup>/g<sub>BOP</sub>; 2.71 mgCd<sup>++</sup>/g<sub>BOP</sub>; and 1.98

429  $mgNi^{++}/g_{BOP}$ .

Final destination of metals laden BOP wastes was the inclusion into lightweight cement mortars formula as a quantitative substitution of the conventional aggregates in consideration of the minimized potential release of metals detected after the water leaching tests carried-out on the consolidated specimens.

434 Moreover, low thermal conductivities  $\lambda$  (0.18 W/mK) of the prepared cement composites were 435 observed as opposite to the conventional sand based control (2.0 W/mK) but the mechanical 436 properties were quite low (~1 N/mm<sup>2</sup>) thus suggesting to introduce in the metals laden mortar other 437 more resistant aggregates in order to employ these conglomerates for non structural lightweight 438 applications (panels, plasters).

439

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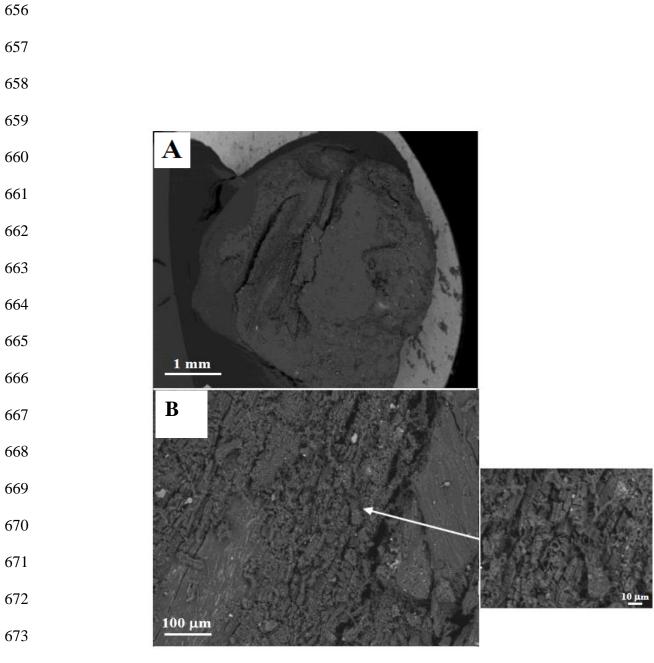
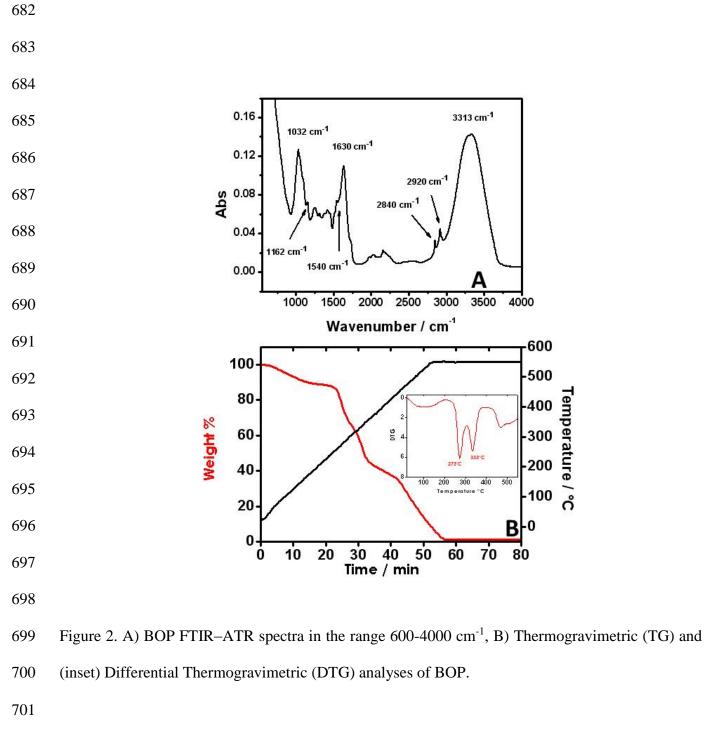
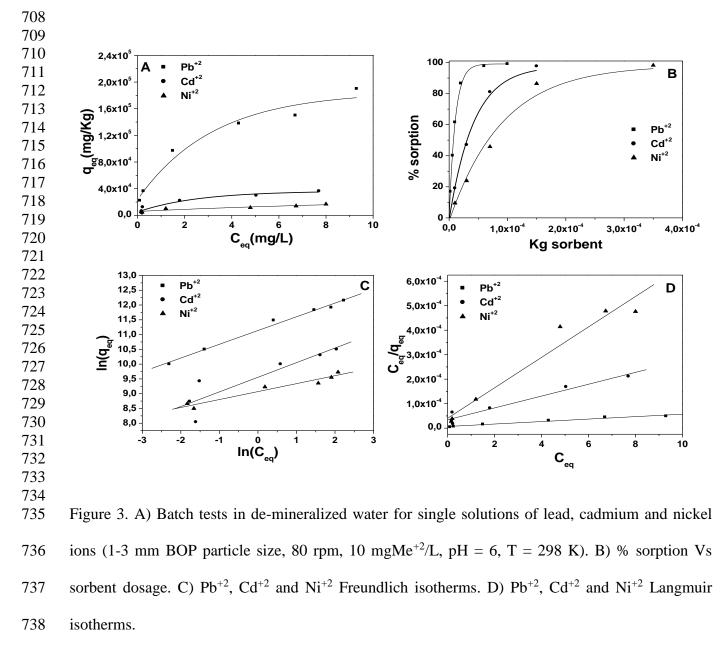
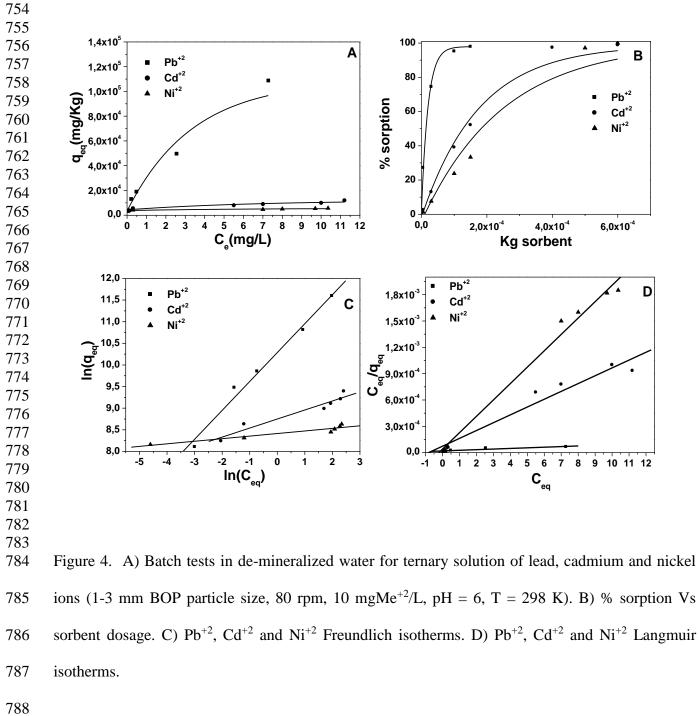


Figure 1. A) SEM back scattered electron images of a single BOP grain; B) BOP texture with the
corresponding magnification. The white grains are silicate minerals, mainly feldspars and less
frequent clay minerals.

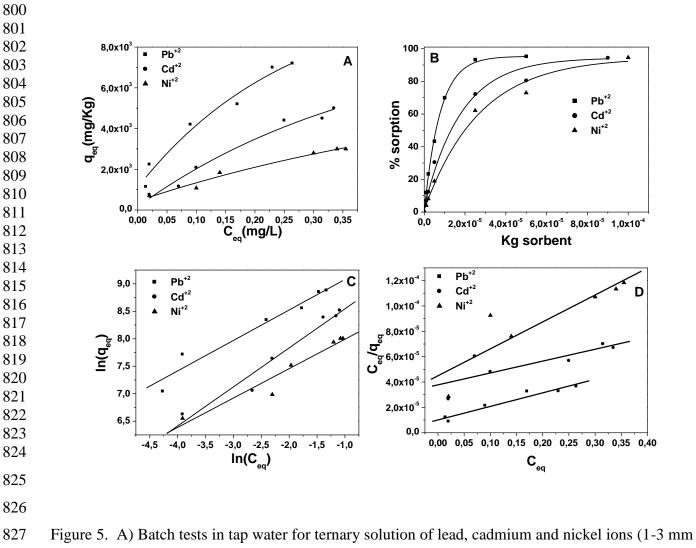


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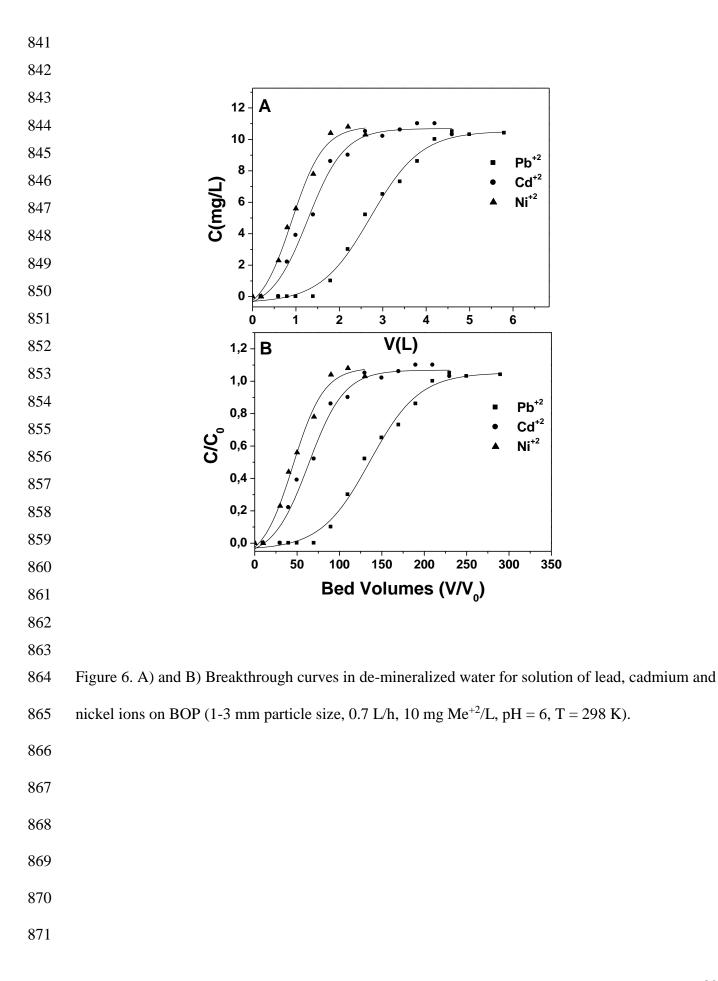




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BOP particle size, 80 rpm, 0.3 mgMe<sup>+2</sup>/L, pH = 7.5, T = 298 K). B) % sorption Vs sorbent dosage. (1)  $Pb^{+2}$ ,  $Cd^{+2}$  and  $Ni^{+2}$  Freundlich isotherms. D)  $Pb^{+2}$ ,  $Cd^{+2}$  and  $Ni^{+2}$  Langmuir isotherms.



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	Ni	13.84	0.83	
882	Cd	19.41	1.09	
883	Pb	46.79	1.39	
884				
885 Figure 7. EDX analysis of a	metal laden BOP aft	er column test i	n ternary solution (	5.5 g BOP. 0.7
			i ternary soration (	

886 L/h, 10 mg Me<sup>+2</sup>/L influent ternary solution, pH = 6, T = 298 K).