



Politecnico di Bari

Repository Istituzionale dei Prodotti della Ricerca del Politecnico di Bari

Overview on recent developments in energy storage: Mechanical, electrochemical and hydrogen technologies

This is a pre-print of the following article

Original Citation:

Overview on recent developments in energy storage: Mechanical, electrochemical and hydrogen technologies / Amirante, R., Cassone, E., Distaso, E., Tamburrano, P.. - In: ENERGY CONVERSION AND MANAGEMENT. - ISSN 0196-8904. - 132:2017(2017), pp. 372-387. [10.1016/j.enconman.2016.11.046]

Availability:

This version is available at <http://hdl.handle.net/11589/92843> since: 2022-06-20

Published version

DOI:10.1016/j.enconman.2016.11.046

Publisher:

Terms of use:

(Article begins on next page)

1 OVERVIEW ON RECENT DEVELOPMENTS IN ENERGY

2 STORAGE: MECHANICAL, ELECTROCHEMICAL AND

3 HYDROGEN TECHNOLOGIES

4 Riccardo Amirante, Egidio Cassone, Elia Distaso, Paolo Tamburrano

5 *Department of Mechanics, Mathematics and Management, Polytechnic of Bari, Italy.*

6 Abstract

7 Energy production is changing in the world because of the need to reduce greenhouse gas
8 emissions, to reduce the dependence on carbon/fossil sources and to introduce renewable
9 energy sources. Despite the great amount of scientific efforts, great care to energy storage
10 systems is necessary to overcome the discontinuity in the renewable production. A wide variety of
11 options and complex characteristic matrices make it difficult and so in this paper the authors show
12 a clear picture of the available state-of-the-art technologies. The paper provides an overview of
13 mechanical, electrochemical and hydrogen technologies, explaining operation principles,
14 performing technical and economic features. Finally a schematic comparison among the potential
15 utilizations of energy storage systems is presented.

16 Keywords: Energy storage; Power system; Technical and economic performance features;
17 Renewable energy systems

18 1. Introduction

19 “Energy” can be considered a prerequisite of the countries development and one of the most
20 important factor to increase people wellness. For this reason the world energy diet shows a steady
21 growth (+56% from 1990 until 2015) in the last years mainly due to the Asian continent (see
22 scenario of Figure 1), while North America and European Union slightly decrease energy demand
23 from 2008 due to the economic crisis. Fortunately, in the last 20 years, energy production from
24 renewable sources has risen continuously (see Figure 2). The Italy scenario is a good further
25 example of energy production due to the great amount of energy plants for renewables
26 production. In fact, Figure 3 shows the Italy trend of energy production in the 2005-2015 interval
27 (data provided by national energy services manager, GSE). The slight decrease in renewables
28 production in 2015 (vs 2014) is due to a minor rainfall in this last year.

29 The reasons that explained this increase of attention about renewables are the lack of carbons and
30 the necessity to offer a best future to 4,5 billion of people who today have a limited access to
31 energy resources, and this also matches the international environment treaties to reduce world
32 pollution, i.e., Kyoto Protocol, EU 2020. Despite this trend, renewable sources are still unable to
33 overcome the other energy sources for mass energy production because of their random
34 behaviour [1–3]. For instance, the biogas production from biomass relies on the performance of a
35 cultivation, but in a more general way, on the employed “digestion” processes [4–6]. Eolic and
36 solar generations are characterized by the greatest availability, but are considered to be
37 unpredictable. An additional important aspect that should be considered is that generally the load
38 curves almost never follow the energy availability curves. Consequently, the direct consumption of
39 energy produced from renewable sources can be very inefficient and inadequate because a large
40 amount of energy is over-produced and then most commonly wasted, as well as, is not directly
41 recovered in other cases (e.g., thermal conversion). This asynchronous production against energy
42 demand can represent a limiting factor to the further development of renewables. The only
43 solution to continue improving renewables is the energy storage. For these reasons the increase in
44 scientific research into energy storage systems is highly desirable. The use of an Energy Storage
45 System (ESS) can raise the energy production efficiency [7,8]. It is charged with energy surplus
46 coming from the production phase, while when the production is insufficient or absent, the
47 needed amount of energy is withdrawn by its discharging. Moreover, such system allows
48 separating, both in space and time, the power production from its consumption.

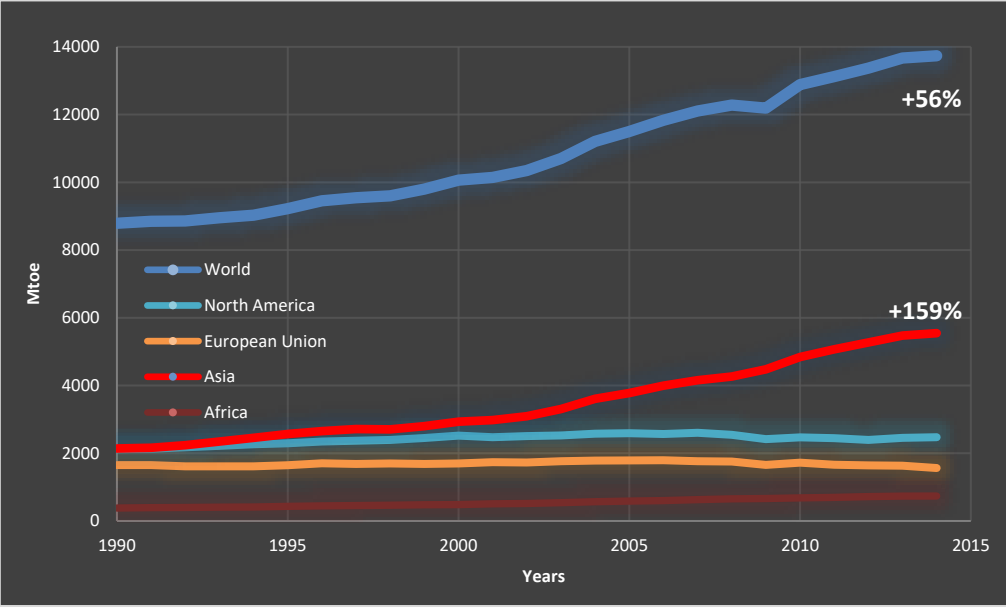


Figure 1 - World energy diet (Mtoe), adapted from ENERGY DATA - Global Energy Statistical Yearbook 2015

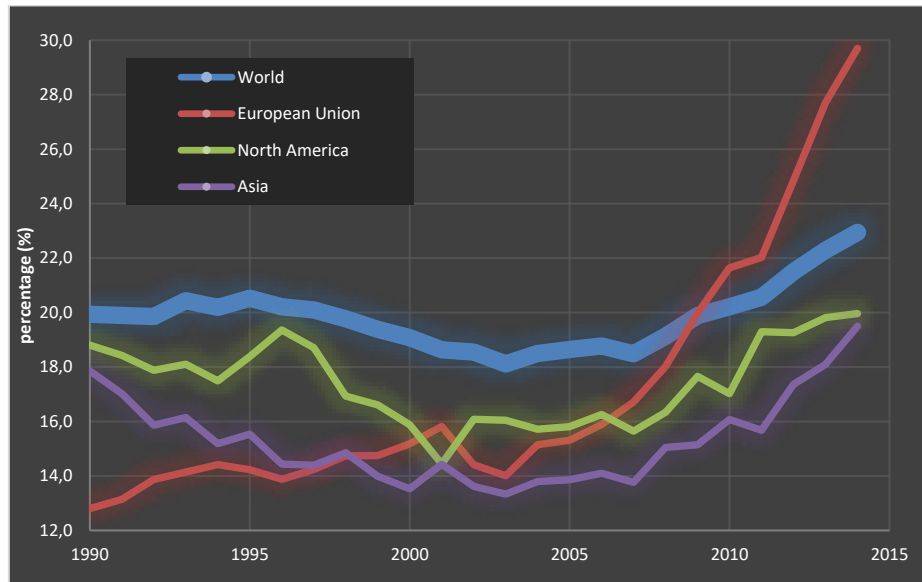


Figure 2 - Renewables to ELECTRICITY production, ENERGY DATA - Global Energy Statistical Yearbook 2015

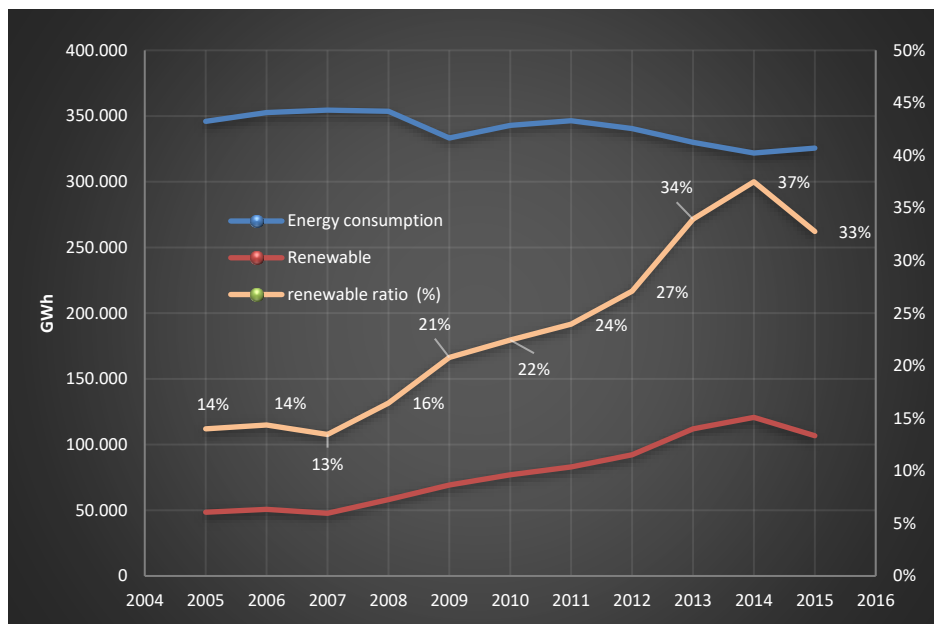


Figure 3 – Italy electric energy demand, GSE data 2015

In this way, it would be possible to achieve the transition from a localized energy production (few big power plants) to a grid energy production (more and smaller power plants). This change would increase the global efficiency of the whole energy production-distribution system, reducing the losses in the Transmission and Distribution (T&D) process and being much more environmental friendly due to the lower fossil fuel consumption and pollution emissions [4].

A huge variety of energy storage systems is available. Usually, it is possible to provide a classification based on the energy conversion mode. Therefore, they can be divided as follows:

- Mechanical Systems: Compressed Air Energy Storage (CAES), Pumped Hydroelectric Storage (PHS) and Flywheel Energy Storage (FES);

- Electric Systems: supercapacitors and Superconducting Magnetic Energy Storage (SMES);
- Electrochemical Systems: Lithium-ion battery and flow battery;
- Hydrogen storage, based on electricity conversion in hydrogen in charge phase and vice versa.

The present work aims to provide an extensive review on mechanical, hydrogen and electrochemical storage systems, which appear to be the most promising and appealing technologies in a long time prospective. In particular, the mechanical systems represent the longest studied storage technology, while the battery storage is largely considered as the technology that today attracts the most profitable investments, both in static applications and automotive field. The hydrogen storage represents one of the most remarkable alternative to the fossil fuels. Starting from the physical principle on which they are based, a detailed analysis on the most recent developments and applications is therefore reported for each of the storage solutions considered in the present work.

2. Mechanical Systems

Pumped hydro storage

In Pumped Hydro (PH) stations, water is pumped to a higher reservoir, during the charging phase, using over-produced energy. During the discharging phase, water flows downfall through the turbine producing energy. A schematic is reported in Figure 4.

Usually, the hydraulic machine is a “pump as turbine” (PaT), a reversible machine that can act both as pump and as turbine. PaTs are connected to reversible electrical reversible machines (Alternator-Motor). In the charging phase, external energy is employed to pump water from the lower reservoir to the upper one. When the power demand is high, the discharge phase starts and the water flows downward through the turbine generating electrical energy. The charge and the discharge powers depend mainly on the hydraulic head (namely from the height difference between the reservoirs), while the amount of energy stored is function of the capacity of the reservoirs [7,9].

Pumped hydroelectric storage is a mature technology that offers a long storage period, high efficiency, relatively low capital cost per unit of energy and fast response time.

The typical rating is between 1000 and 3000 MW. The discharge period takes hours or days and the response time is less than 1 minute. The lifetime is about 40 years while the power and energy capital cost value amount respectively to 500-1500 €/kW and 10-20 €/kWh [9–11].

If the losses within the pipeline are neglected, the efficiency depends directly on the machine's efficiency and a typical value is comprised between 70% and 80%. The most performing systems reach an efficiency of 87% [10].

The main drawbacks are represented by the geological structure reliance, the low energy density (0,3 kWh/m³), the long construction time (about 10 years), the high capital cost (millions of euros), together with some environmental issues linked to the building of the reservoirs [12–14]. Moreover, evaporation losses are significant and they increase the costs in the hot climate [7,13].

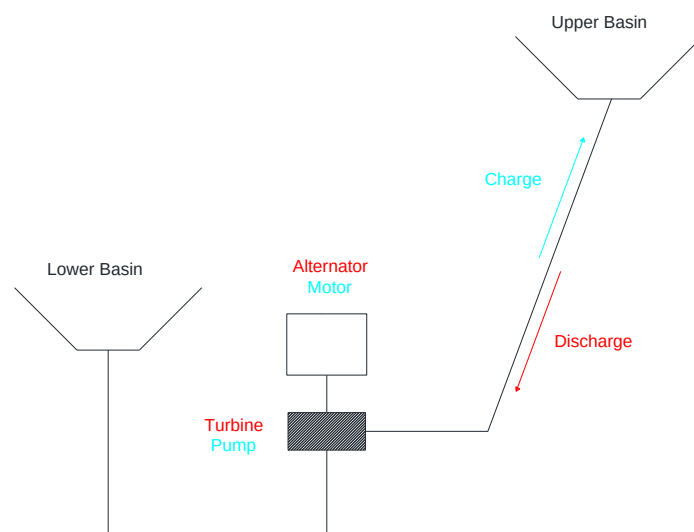


Figure 4 - A pumped hydro storage system [11].

PHS represent the oldest storage technology: in Alpine region hydroelectric systems were built since 90s of XIX century. In 1950s reversible pumps-turbines were introduced. Nowadays, PHS stores about 127 GW worldwide (more than 76 GW were installed just in 2014), which corresponds to 3% of the global energy storage capacity. About 99% of the stored energy is "packed" in water [10,11]. Moreover, PHS results suitable for balancing intermittent energy generation from wind or photovoltaic plants. Especially in isolated realities, as Canary Islands or Ikaria Islands, PHS coupled with wind power represents the best solution if containing costs is a main purpose [10,12,15–17]. In such contexts the sea is used as lower reservoir, saving part of the construction costs. As side effect, more attention preventing corrosion is needed [16,18–20].

Recently, Sarasúa et al. [21] provided an example about the importance that hydropower plants can have in the grid integration of increasing levels of intermittent energy sources. They studied the dynamic response and governor tuning of a long penstock pumped-storage hydropower plant (PSHP) equipped with a pump-turbine and a DFIG, which was connected to a small isolated power system with thermal generation, and which provided load–frequency control under the orders of an automatic generation control (AGC) system. Three different criteria were investigated for

119 tuning the unit's governor. The first two criteria (DCP and FDR) were based on the root locus
120 analysis of a linearized 4th order model of the unit's speed control loop. The third criterion was
121 based on a Pareto approach using the non-linear model. They found that FDR tuning criterion
122 managed to significantly damping the oscillations of both the hydraulic and mechanical variables
123 of the PSHP, which may result in an extension of the plant's lifetime. By contrast, it gave rise to a
124 higher overshoot in the unit's speed, what is not likely to affect the output power of the PSHP or
125 the system frequency. With the DCP tuning criterion, the dynamic response of the PSHP was
126 poorly damped. The Pareto-based tuning criterion showed an intermediate behaviour in terms of
127 both the damping and overshoot of the hydraulic and mechanical variables of the PSHP.
128 However, the influence of different values of the reference unit speed, should be so studied too, in
129 order to verify the adequacy of the governor tuning criteria for variable-speed operating
130 conditions.

131 Talking about photovoltaic and wind systems used in rural electrification, the great part of the
132 works, in which to find an efficient way of storing energy is the main topic, have not considered
133 other ways of storing energy except for conventional battery storage systems. Kusakana [17],
134 showed as a hybrid system consisting of a photovoltaic unit, a wind unit, a pumped hydro storage
135 system and a diesel generator can be an attractive solution. In such study, an energy dispatch
136 model that satisfies the load demand, taking into account the intermittent nature of the solar and
137 wind energy sources and variations in demand, is presented, with the aim to minimize the hybrid
138 system's operation cost while optimizing the system's power flow considering the different
139 component's operational constraints.

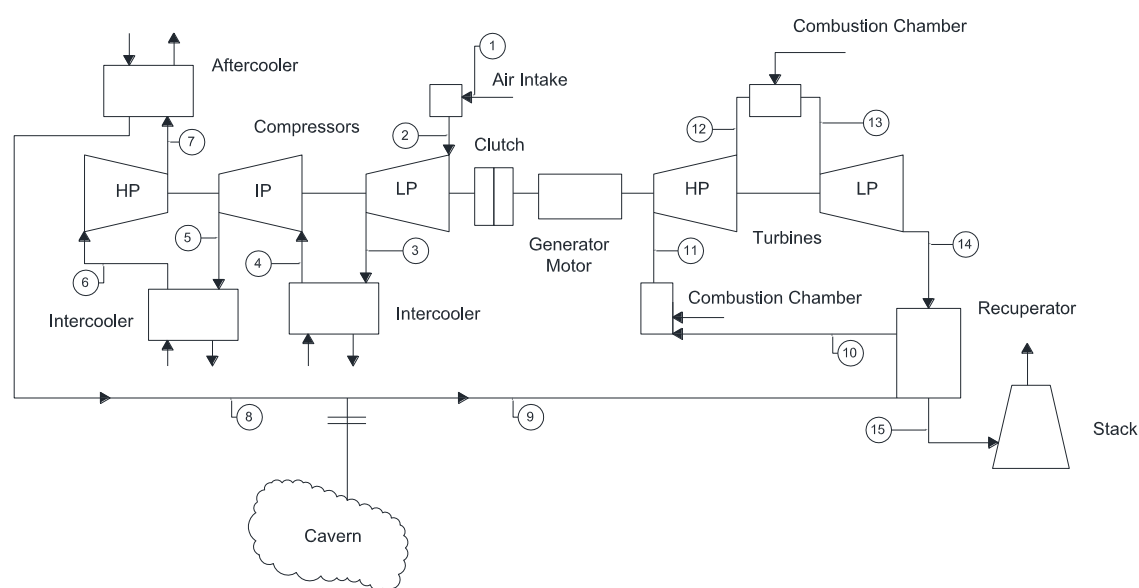
140 The integration of wind or solar farms and pump storage plants is instead increasing. More and
141 more large-scale renewable energy integration systems are taking shape gradually. As a
142 consequence, optimized control has become a great challenge to these systems. Reversible design
143 and "S" characteristic area of the PSHU are the basic obstacles [22,23]. Operating along the S-
144 shaped curve can lead to intense oscillations of rotational speed in the start-up process making it
145 is so unstable that it may cause difficulties with synchronization. An accurate care is needed to
146 control systems applied to renewable energy plants to avoid the so called "voltage dips" to the
147 grids. Thus, this scenario might be attractive for a research field that takes into account innovative
148 controlling techniques. An example could be the proposal of that used a Fuzzy logic rules as a
149 control for turbo-gas technology [24]. Recently, Xu et al. [25] studied this problem and proposed
150 an adaptively fast fuzzy fractional order PID (AFFFOPID) control method for PSHU. In their work an
151 improved stochastic search algorithm, namely BCGSA, and the time domain optima tuning
152 function are proposed for the parameter selection of PSHURS. And, by means a comparative

analysis among the AFFFOPID, PID and FOPID method of the novel PSHURS (which could fully reflect the nonlinear in 'S' area) Thy showed that AFFFOPID could effectively restrain the oscillation of rotational speed in 'S' area of PSHU and has high robustness and stability. Conversely, the introduction of Hydrokinetic micro-turbines lowered the PHS target size, allowing the construction of smaller plants with lower capacity. As a result, this energy storage system became suitable also for grid application as well as for little realities [17,20].

Compressed air energy storage

In the Compressed Air Energy Storage (CAES) systems, the energy is stored in form of pressure energy, by means of a compression of a gas (usually air) into a reservoir. When energy is required, the gas is expanded in a turbine and the energy stored in the gas is converted in mechanical energy available at the turbine shaft. A possible system configuration is depicted in Figure 5. A usual plant arrangement is composed of a multistage compressor equipped with both an intercooler and an aftercooler, a multi-shaft gas turbine, a motor/generator with a clutch, which allows to act the compressor and the turbine in different moments, an underground storage for the compressed air and other equipment controls and auxiliaries, such as a fuel tank and a heat exchanger [1–3,5–7,10].

In the charging phase, the exceeding energy is used to compress air in the underground storage (up to 70-100 bar). In the discharging phase, the air is drawn from the storage, heated (burning natural gas or using recovered/recycled heat) [1,3], and then expanded through the turbine train [4,9,13,14].



173

174

Figure 5 - Schematic diagram of a CAES plant, adapted from [20]

175 CAES is suitable for large-scale power, i.e., hundreds of MW. T storage period can be greater than
176 a year. The efficiency varies between 70% and 89% since it is correlated to the compressor and
177 turbine efficiencies and it is decreased by low self-discharge ability that is typical of this system.
178 Other peculiarity are a fast start-up (9 minutes for an emergency start, 12 in normal conditions),
179 an energy density counts about 12 kWh/m³, a lifetime approximately of 40 years (comparable to
180 PHS) and a power capital costs that range from 400 €/kW to 800 €/kW (since the presence of
181 underground storage conditions)[9,11–13].

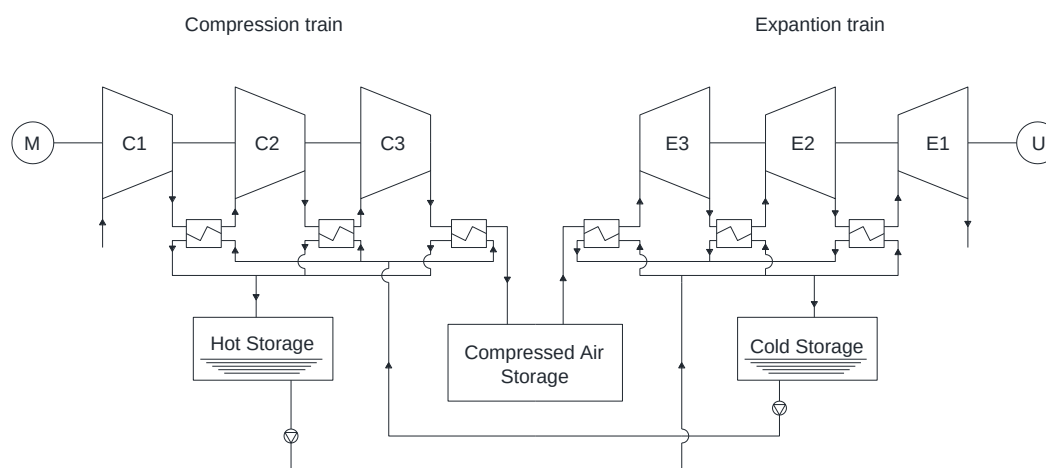
182 Thanks to these features, CAES results suitable for energy management applications as load
183 shifting, peak shaving, frequency and voltage control [9].

184 Furthermore, for adiabatic CAES, heat usually cannot be efficiently utilized and the low inlet
185 temperature of turbine in an adiabatic-CAES (A-CAES) usually leads to low discharge efficiency. To
186 address these problems, Yao et al. [26] recently proposed a novel combined cooling, heating and
187 power system (CCHP) based on small-scale CAES. In particular, a gas engine was employed to
188 boost the power output, while the tri-generation aimed at using heat, particularly low-grade heat
189 in a cascade way. They performed a sensitivity analysis that showed that the air temperature and
190 pressure at the turbine inlet, as well as the effectiveness of the heat exchangers have great
191 influence on the system's thermodynamic performance. In such study, the trade-off between the
192 thermodynamic and economic performances was also investigated by an evolutionary multi-
193 objective algorithm. The results they showed reported that the total investment cost per output
194 power of the Pareto solutions does not increase significantly when increasing exergy efficiency
195 below 51%, indicating the solutions with an exergy efficiency of around 51% are promising for
196 practical designs.

197 The most important drawback of CAES technology is represented by the difficulty in finding
198 appropriate geographical sites with underground natural caves. Moreover, fossil fuel are burned
199 within the system and this raises concerns about the well know problems relate to pollutant
200 emissions [12,27].

201 Therefore, in order to deal with these issues, Advanced Adiabatic CAES (AA-CAES) systems have
202 been developed. Referring to Figure 6, the thermal energy is drawn from the compressed air,
203 stored in the thermal storages, and released before the expansion, without requiring any
204 combustion process and therefore involving no fuel consumption. The compressed air is stored in
205 stainless steel vessels in place of natural caves [27–30]. In this way it was also possible to
206 implement the so called Sm CAES (SS-CAES) since they generate smaller power, namely less than
207 10 MW [7,28]. SS-CAES plants are also built using external reservoirs instead of natural caves.

208 Furthermore, it may be possible to recover a greater part of the wasted heat, by using a Kalina
 209 cycle enhancing the cycle efficiency by 4% [29]. The Kalina cycle is a combined cycle that employs
 210 a two phase solution of two fluids with different boiling points. Since the solution boils over a
 211 range of temperature more of the heat can be extracted from the source than with a pre working
 212 fluid and different level of heat sources can be used in the same system. Such cycle requires,
 213 however, a more complex plant.



214
 215 *Figure 6 - CAES-TES plant, adapted form [21]*

216 The oldest CAES plant was built in Hundorf, Germany, in 1978. It was designed to meet the energy
 217 demand peak and allowing a nuclear power plant to maintain a constant capacity factor. The plant
 218 used two salt dome caverns as underground storage (300000 m^3 at 50°C and 46-66 bar) and
 219 developed 290 MW [28–30]. The MacIntosh plants, built in 1991 in Alabama with 110 MW of
 220 energy storage, improved the Hundorf's technology by using a heat recovery system to recycle
 221 part of the heat that the gas still has once it left the turbine [28,29].

222 A variant of CAES is represented by the Liquid Air Energy Storage (LAES). In that system an air flow
 223 is liquefied and then stored at atmospheric pressure in an insulated vessels [28]. The use of an
 224 external reservoirs, instead of that of an underground caves, for large scale CAES reduces
 225 significantly the pressure losses due to the rocks natural permeability, increasing the global
 226 efficiency of the system [31].

227 Furthermore, CAES systems are suitable for being integrated with wind turbines both in on-shore
 228 [30] and in isolated areas [31,32] and in off-shore [33] plants as well. It is also possible to
 229 combine PHS with CAES systems, allowing to overcome the respective drawbacks and
 230 consequently producing an increase of the energy density as well as an increase of the efficiency
 231 of the plant [33,34].

232 The most recent innovations in this field include the use of either supercritical compressed air [35]
 233 or compressed CO_2 energy storage system under supercritical and transcritical conditions [36].

234 are represented by Another solution is represented by supercritical compressed air energy storage
235 (SC-CAES) which possesses the advantages of high efficiency by employing the special properties
236 of supercritical air. Recently, Guo et al. [35], targeting the problems of conventional CAES,
237 investigated the performance of a novel SC-CAES. They provided an exergy analysis of the system
238 and concluded that the processes of the larger exergy destruction include compression,
239 expansion, cold storage/heat exchange and throttle.

240 The efficiency of SC-CAES is expected to reach about 67.41% when energy storage pressure and
241 energy releasing pressure are 120 bar and 95.01 bar, respectively. At the same time, the energy
242 density is 18 times larger than that of conventional CAES [35].

243 Liu et al. [36] proposed the use of a two-reservoir of compressed CO₂ energy storage system
244 under supercritical and transcritical conditions. Results showed that the transcritical compressed
245 CO₂ energy storage system has higher round-trip efficiency and exergy efficiency, and larger
246 energy storage density than the supercritical compressed CO₂ energy storage. However, the
247 configuration of supercritical compressed CO₂ energy storage is simpler, and the energy storage
248 densities of the two systems are both higher than that of CAES, which is advantageous in terms of
249 storage volume for a given power rating.

250 *FLYWHEELS*

251 In the Flywheel Energy Storage (FES) systems (Figure 7), it is possible to store the exceeding energy
252 by means a conversion into a kinetic energy of a spinning mass. FES systems are composed of a
253 steel or composite rotating mass (the flywheel) matched up with an electrical motor/generator for
254 charge/discharge phases, two magnetic bearings that avoid mechanical friction and a vacuum
255 chamber able to reduce the aerodynamic losses [11,12].

256 During the charge phase, the flywheel is accelerated by the electric motor; when the energy
257 demand is high, the flywheel slows down and the energy transfer to the generator is realized by
258 electromagnetic induction [9,12].

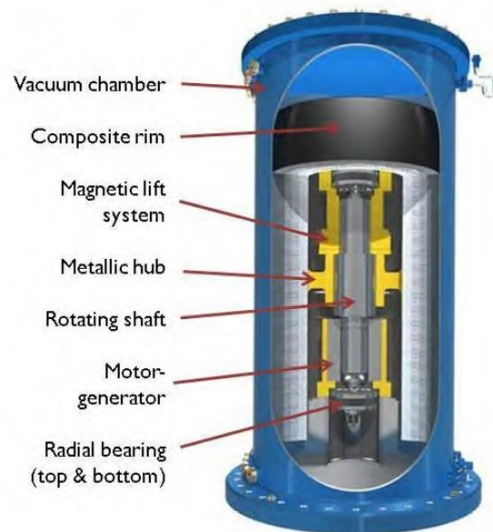


Figure 7 - A typical flywheel configuration-Beacon Power

The stored energy depends on the moment of inertia of the spinning mass, as well as of the rotational speed. Therefore, in order to increase the available energy, it is possible either by increasing the moment of inertia or by using composite materials to build the flywheels that can allow to overcome 10^5 rpm. In fact, the first strategy is typically adopted in low speed applications (speed lower than $6 \cdot 10^3$) while advanced materials are used to perform high speed FES [9,37].

In particular, in order to obtain higher flywheel energy densities, a search for a higher strength and lower density composite for the constant stress portion is required. Recently, Conteh and Nsofor [38] studied lamina and laminate mechanical properties of several composite materials suitable for flywheel energy storage. Design and stress analysis were used to determine the maximum energy density and shape factor for the flywheel. They found that a hybrid composite of M46J/epoxy-T1000G/epoxy for the flywheel exhibited higher energy density when compared to known existing flywheel hybrid composite materials such as boron/epoxy-graphite/epoxy.

These systems can be compared with electrochemical batteries, since they show high efficiency (90-95%), long lifetime (20 years) with low maintenance, no depth-of-discharge effects, no environmental issues deriving from no use of toxic materials, fast response time and short recharge time. Moreover, the flywheels are able to be connected in parallel, increasing the specific energy from low (5 Wh/kg) to high speed (100 Wh/kg) [9,13,14,37].

A critical aspect of this technology is represented by the high self-discharge tendency: frictions and aerodynamic losses can reach about 20% of the stored capacity per hour [11].

FESs find applications both in stationary and vehicular fields. On one hand, flywheels are often coupled with wind-diesel or PV-diesel plants, like UPS units, in order to contain cost and downsize the diesel generator reducing fuel consumption and emissions; moreover FES systems provide

284 backup power, improve power quality, generate high voltage and supply both active and reactive
285 power to compensate frequency and voltage [37,39]. On the other hand, flywheels are often part
286 of hybrid energy storage systems, especially in automotive applications. In these configurations,
287 FES are coupled with batteries: the flywheel represents the power source for transients while the
288 battery provides the main energy storage. Furthermore, KERS (Kinetic Energy Recovery System)
289 relies on FES plant: braking action makes flywheel spin at almost 60000 rpm, providing the engine
290 stop and allowing a 25% reduction in fuel consumption [7,40–42].

291 Recent developments regards innovative electric motors [43] and magnetic bearings based on
292 REBCO (Rare Earth Barium Copper Oxide) HTS magnet, which allow 7-10 tons flywheels spinning at
293 6000-9000 rpm and providing about 1000 kW of power output and about 300 kWh of stored
294 energy [44].

295 Other innovations regard control strategies. Based on the use of a homopolar synchronous
296 machine in a FES, Amodeo et al. [45] developed a high performance model-based power flow
297 control law using the feedback linearization methodology, which is based on the voltage space
298 vector reference frame machine model. The result is a high-performance sensorless control that
299 uses a load angle observer that can be implemented without major hardware modifications or
300 cost increase. Hamzaoui et al. [46] analysed two control techniques DTC (direct torque control)
301 and DPC (Direct power control) dedicated to a variable speed wind turbine based on a double fed
302 induction generator with storage in order to achieve better performance. They showed that the
303 command DTC applied to the DFIG (Doubly Fed Induction Generator) and FES, presented a high
304 performance torque control and a very important dynamic, while keeping good accuracy of
305 control.

306 3. Electric and electrochemical systems

307 *Supercapacitors and magnetic field energy storage*

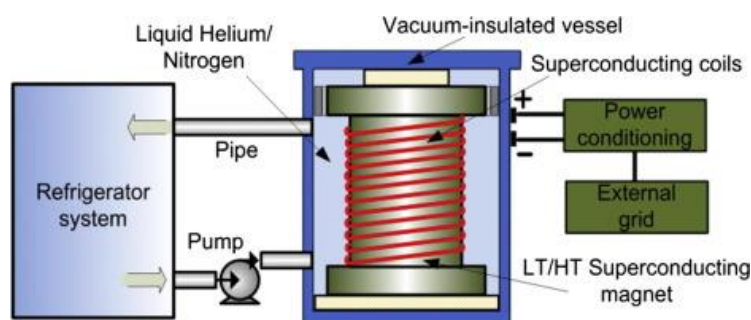
308 Supercapacitors Energy Storage (SES) power plants employ high energy density capacitors to store
309 electricity. Thanks to their fast response, such systems are often employed in power leveling or
310 power balancing installations. An interesting application of SC is given in the work by Zhang et al.
311 [47]. A system to produce electric energy from vibrating railroad is presented: Supercapacitors are
312 employed to store the electricity produced by the generator. Thanks to their fast response, SC are
313 the only devices able to handle a so high power rate. The overall efficiency of the system is about
314 55%, which is an impressive value. Despite the high cycling life, over 10^5 complete cycles, and high
315 efficiency , 84% ÷ 97%, the self-discharge rate (up to 40%/day) and costs (6000 \$/kWh) make this

316 technology still un-able for spread. Research is focused on the development of low cost multi-layer
317 supercapacitors employing new materials like Carbon[9],[48], Graphene [49] or Paper [50] .

318 Hybrid configuration and molecular engineering are also employed. Varying the carbon activation
319 process or the carbon nano tubes (CNTs) orientation, different results are obtained. With random
320 CNTs orientation, a 102 F/g capacitance is obtained; vertically aligning CNTs through a CVD
321 process, the specific capacitance enhances to 365 F/g. Electrode production with chemically
322 activated Carbon gives a specific capacity of 135 F/g while employing a laser, a value of 276 F/g is
323 obtained [51].

324 Hybrid configuration are considered when the major object is pseudocapacitance enhancing. An
325 electrode made of a MnO_2 coated Carbon fiber fabric is presented by Cakici et al. [52]. Results are
326 quite interesting, sicne they showed that capacitor achieved a specific capacitance of 467 F/g with
327 a capacitance retention of 99.7% after 5k cycles. The energy density was 20 Wh/kg. The coulombic
328 efficiency kept around 97% during the 5k cycles of testing. Due to the low cost and the excellent
329 energy density, they concluded that represented a good starting point for new hi-capacity
330 portable energy device.

331 Superconducting Magnetic Energy Storage (SMES) is based on a magnetic field obtained by current
332 circulation in a superconducting wire. A simple scheme is showed in Figure 8



334 *Figure 8 - A typical SMES layout [9]*

335 Electricity come to the coil passing through a power conditioning system (usually an AC to DC
336 converter), then is converted to magnetic field. When discharging, the electric current runs from
337 the coil to the grid converted by a DC to AC converter.

338 To reduce ohmic losses, the wire is kept under it is superconductive temperature. Now a class-
339 based distinction can be made:

340 High Temperature SMES' coil works at $\sim 70\text{K}$ while in Low Temperature SMES coil is kept at $\sim 7\text{ K}$.

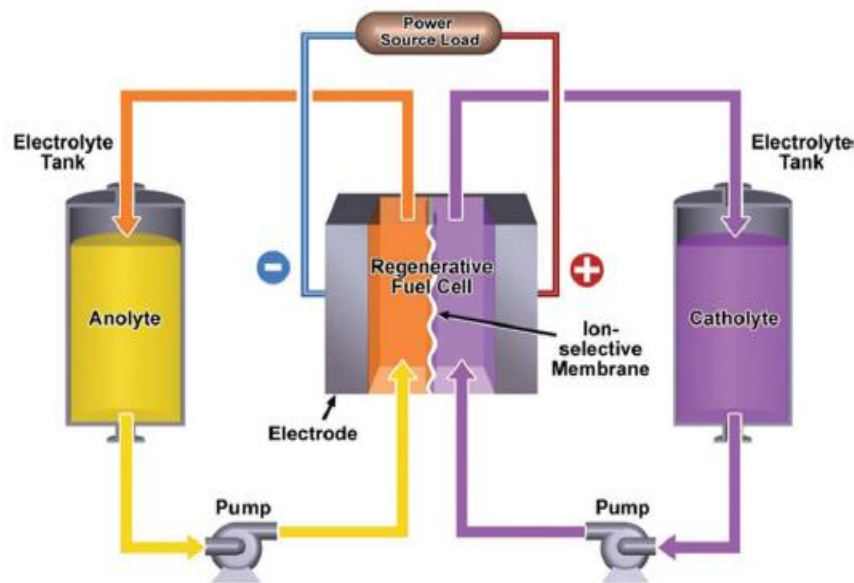
341 Such systems can achieve high energy densities (up to 4kW/l), very high efficiencies (95% ÷ 98%),
342 fast response times (milliseconds) and very good lifetime (up to 30 years). They can even be fully
343 discharged without reporting significant deterioration, despite almost all batteries. Moreover, high
344 shunt currents are supported so high powers can be handled (for short times) without damages.
345 However, the cost are still forbidding, being around 10.000 \$/kWh, due to the cooling system and
346 coil's materials. Environmental issues rises from high concentrated magnetic field employing [9].

347 SMES and Supercapacitors can be used in hybrid configuration with Batteries in contexts where
348 power demand often changes respect the power production (e.g. Wind and Photovoltaic farms),
349 combining the high power density of SMES and SES with the high energy density and reliability of
350 batteries [53–55]. Introducing a Proportional-Integral (PI) controller, Prakash et al. obtained a
351 lower frequency variation in various hybrid configurations, even in absence of storage systems.
352 The lowest frequency variations are obtained employing fast response EE systems such as
353 Flywheels and Supercapacitors. Moreover, it's exposed that systems' response is faster when
354 energy is transferred to employers by a High Voltage Alternated Current link, which is optimal for
355 distances lower than 50 km. In this case (FESS+SES) the Integral Square Error of the frequency
356 variation – in the worst condition analysed (wind turbines + fuel cell + photovoltaic + diesel
357 generation)- decreases from 0.2360 to 0.0194. Even in High Voltage Continuous Current link the PI
358 controller introduction strongly reduces the system's response time [56]. Another application of a
359 PI controller is given in [57]. A STATCOM controller is employed to guarantee the grid stability
360 against the reactive power variation due to the varying speed of wind turbines and variable
361 torque request of induction machines. The bidirectional AC/DC converter (STATCOM) connected
362 to the grid and coupled with a supercapacitor is able to achieve the requested reactive power in
363 order to maintain stable the whole grid. Moreover, the Supercapacitor achieve the controller the
364 ability to satisfy the active power request in transient stages. It can be seen that the storage
365 system is not the only entity involved in a micro-grid structure. The energy management policy
366 plays a crucial role too.

367 *Redox flow battery*

368 Redox Flow Batteries (RFB) are a new generation of power accumulation units. Their biggest
369 advantage is that the power density is detached by the battery's capacity, allowing the easy
370 upgrading of existing RFB supplies and various configurations depending on specific requests.
371 Despite standard batteries, the redox reaction is performed through an ion-permeable membrane
372 dividing the positive and negative electrolyte. The electrolytes are stored in separate tanks. They
373 are pumped into the cell and the proton exchange between anode and cathode generates the

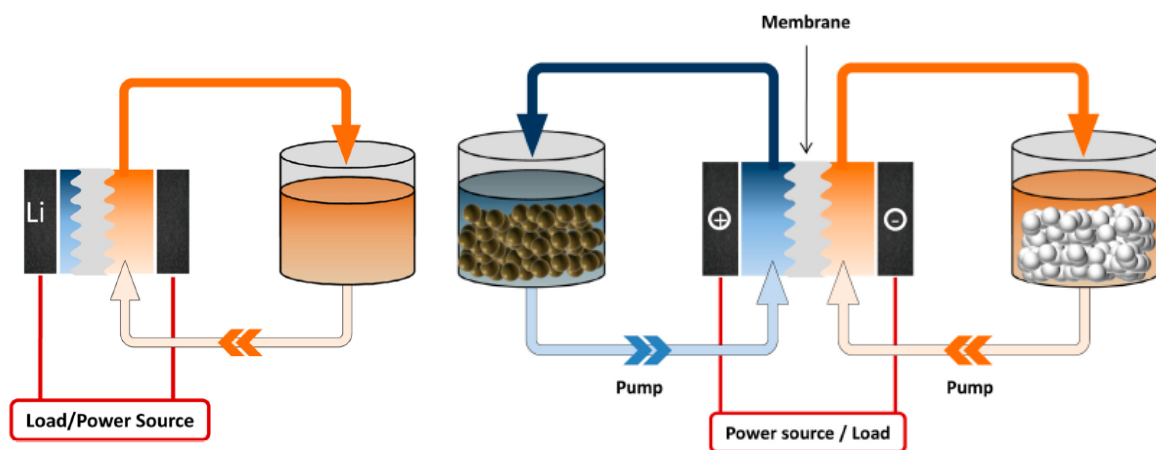
374 electric power circulation. The tank capacity is directly related to the battery's capacity while the
375 number and materials of cells influences the battery power capabilities.



376

377

Figure 9 - A standard RFB configuration



378

379 Figure 10 - Hybrid configurations: left is with a solid electrolyte (Lithium typically) right a semi-solid configuration (the
380 solid material, Lithium, is stored in tanks with the liquid electrolyte).

381 Basic operative parameters are the usual of common batteries like Energy (or equally Power)
382 Density (ED), the various efficiencies (Coulombic, Voltmetric and Energetic) and of course Capacity
383 and life (expressed in terms of time or cycles).One of the most important differences between
384 RFBs and common electro-chemical power accumulator units is the relationship between Depth of
385 Discharge (DoD) and life-time. Liquid RFB's life is generally not influenced by the Depth of
386 Discharge (DoD) (full Vanadium and Zinc-Bromine RFB, for instance, can achieve a 100% DoD
387 without losing life-cycles or Efficiency). It should be pointed out that cell's life and efficiency
388 depends on various factors like the operating temperature and the discharging current [58].

389 An ideal battery should have high Energy Density (or equally high Power Density) to reduce the
390 overall dimensions (and/or weight), of course great Capacity and high Energy Efficiency. Output
391 voltage and/or current is not so important because cells may, however, be connected to achieve
392 higher Current gain (e.g. parallel connection) or higher Voltage Output (e.g. in series connection).
393 The second choice is less typical due to fast electrodes degradation phenomena.

394 Depending on battery type, typical energy density values are in the order of 45-90 Wh/l (full
395 Vanadium RFB) [59].

396 The major cons in RFB are the low specific energy density and high costs. To enhance energy
397 density and overall efficiency, different approaches have been followed. New redox species have
398 been tested, including Lithium, Sulfur and Quinones. Moreover, molecular engineering has been
399 applied to create organic specific molecules and ligands (Metal or organic complexes) to avoid
400 toxicity or corrosion related troubles and to improve energy density. The introduction of Carbon
401 Nano Tubes (CNT) yielded higher efficiency and higher capacity, due to lower electrode's ohmic
402 losses [59]. Electrode material, form and coating has a general heavy impact on battery's
403 performances.

404 Treating standard electrodes in a partial oxygen environment (42% of Oxygen, 58% Nitrogen)
405 decreased the activation over potential of 140 mV, moreover an aerial increase was obtained. The
406 Energetic Efficiency (EE) raised from 63% to 76% and the usable capacity at 200 mA/cm² has
407 almost doubled. So doing, system cost has been reduced of about 20% (at constant stored energy)
408 [60].

409 Employing Nitrogen-Doped Carbon Nanotubes as electrodes, the EE increase up to $\approx 76\%$ while
410 the discharge capacity raises from 25 to 33 Ah/l (@40 mA/cm²)[61].

411 Electrodes (Graphite felts) modified with atmospheric pressure plasma jet can achieve a 22% EE
412 improvement [62].

413 A coconut shell derived mesoporous electrode is presented by Ulaganathan et al. Such electrode
414 provides an extra electron couple reaction in the cell (V^{3+}/V^{4+}) bringing the cell EE to 85% after
415 100 cycles [63].

416 In flow-by configuration, the employment of perforated carbon paper electrodes yielded higher
417 power and current densities, with a general performance increase up to 31%, with a global lower
418 pressure drop ($4 \div 14\%$) [64].

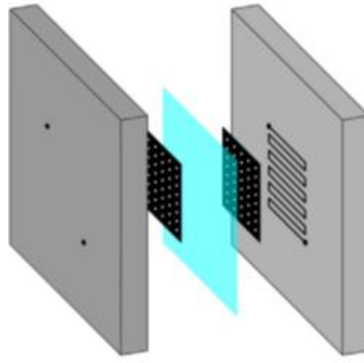


Figure 11 - The cell used in [64]

Membranes too are elements of research. Jia et al. introduces an innovative (and low cost) Sulfonated Poly(Ether Ether Ketone) (SPEEK) membrane embedded with the short-carboxylic multi-walled carbon nanotube (shortly SPEEK/SCCT membrane) claiming an overall performance increase (7% higher Coulombic Efficiency -CE-, 6% higher EE but lower capacity loss in comparison with the one with Nafion 212)[65].

In Xi et al.'s work the SPEEK membrane is analyzed varying the Degree of Sulfonation (DS) and casting solvent showing interesting results [66]:

- with a 67% DS the ion selectivity is optimal;

- N,N' -dimethylformamide (DMF) is the optimum casting solvent due to polymer (membrane itself)-solvent interaction .

CE increases by 5,4% and EE by 6,6% respect the Nafion 212 [66].

The employment of a hybrid membranes (SPI/ZGO) composed of Sulfonated PolyImide (SPI) and Zwitterionic polymerfunctionalized Graphene Oxide (ZGO) shows a higher cell performance (CE: 92-98%, EE: 65-79%) compared with commercial Nafion 117 membrane (CE: 89-94%, EE: 59-70%) at 30-80 mA/cm²[67].

A Diels Alder Poly(Phenylene) (DAPP) membrane is instead analyzed by Pezeshki et al. [68] that showed as, depending on the functionalization group, DAPP could be used as anion exchange membrane or cation exchange membrane. Energy Efficiency raised to 85 % while CE is slightly above 95% .

Sol-gel-derived Nafion/SiO₂ hybrid membrane lowers vanadium ions permeability and increases Coulombic and Energy efficiencies compared to pure Nafion membrane. The pore size and pore-size distribution of Poly(Ether Sulfone) (PES)/silica composite porous membranes can be

controlled by the amount of silica gels inside the pores to reach a Coulombic Efficiency of 97% [69].

A pump-less solution, based on a hybrid electrolyte, has also been tested (Lithium-Polysulfide) [70] with up to ≈ 400 Wh/kg Energy ED [70]. A membrane-less battery (Lithium-Ferrocene) is proposed in [71]; ED is about 40Wh/l . A general description of new conception RFB and redox species can be found in [59,72]. Currently, Lithium is the principal candidate to enhance RFBs' Energy Density, with the anode degradation phenomena. One interesting application is reported in [73] where a very cheap and durable RFB is presented. Although the low ED (10 Wh\l) the battery life is high (10k cycles).

A solar-driven chargeable Lithium–Sulphur battery can be obtained with a Pt-modified CdS photocatalyst. Sulphur is oxidized to Polysulphide in aqueous solution, so doing electro-chemical energy and Hydrogen is produced. Battery can deliver a specific capacity of 792 mAh g⁻¹ during 2 h photocharging process with a discharge potential of around 2.53 V versus Li⁺/Li. Charging can be performed at direct sunlight [74].

Despite the high number of publications regarding RFBs, the major adopted are still the full Vanadium, Zinc-Bromine and Iron-Chromium RFBs. In the following Table 1, Table 2 and Table 3 the estimated costs are expressed [75]. Zinc-Iron too is an emerging technology in wide energy application (ViZn projects). A target cost of 100 \$/kWh is achieved by a combination of inexpensive redox materials (i.e., zinc and iron) and high cell performance (e.g., 676 mW/cm² power density) [76].

Table 1 - Main cost items of VRFB systems - ^a Including BOP costs approximately 25€/kWh; ^b Mainly for MW-scale systems with rated DoD of 80%, used for bulk energy storage and T&D support (discharge time 4h); ^c Every 8 years for the mentioned application (365-500 cycles per year).

Cost item	Average	Middle fifty range, IQR	Range
PCS ^a (€/kW)	490	478-518	472-527
Storage section ^b (€/kWh)	467	440-536	433-640
Fixed O&M (€/kWh-yr)	8,5	4,3-16,1	3,4-17,3
Variable O&M (€/MWh)	0,9	0,5-1,2	0,2-2,8
Replacement costs ^c (€/kW)	130	114-165	111-192

Table 2 - Main cost items of zinc-bromine (Zn-Br) battery systems - ^a Including BOP costs approximately 25€/kWh; ^b Mainly for MW-scale systems with rated DoD of 80%, used for bulk energy storage and T&D support (discharge time 2-5h); ^c Every 15 years for the mentioned application (365 cycles per year).

Cost item	Average	Middle fifty range, IQR	Range
PCS ^a (€/kW)	444	343-470	151-595
Storage section ^b (€/kWh)	195	178-314	178-530
Fixed O&M (€/kWh-yr)	4,3	3,6-5,4	3,2-6,9

Variable O&M (€/MWh)	0,6	0,4-1,0	0,3-2,0
Replacement costs ^c (€/kW)	195	148-198	101-201

470

471 *Table 3 - Main cost items of iron-chrome (Fe-Cr) battery systems - ^a Including BOP costs approximately 25€/kWh; ^b*
472 *Mainly for MW-scale systems with rated DoD of 80%, used for bulk energy storage and T&D support (discharge time 2-*
473 *5h); ^c Every 15 years for the mentioned application (365 cycles per year).*

Cost item	Average	Middle fifty range, IQR	Range
PCS ^a (€/kW)	362	333-393	326-525
Storage section ^b (€/kWh)	145	126-152	64-156
Fixed O&M (€/kWh-yr)	3.3	2,8-4,0	2,7-6,9
Variable O&M (€/MWh)	0,4	0,2-0,6	0,1-1,0
Replacement costs ^c (€/kW)	29	24-33	14-38

474

475 *Lithium battery*

476 Lithium-ion battery is a market widespread technology, especially for low power portable
477 application since the first steps of the development in the early 1990s [13,77].

478 Nowadays, this kind of battery is available also for higher power applications, both for automotive
479 and stationary purpose [9].

480 Generally, two electrodes and an organic electrolyte compose a Lithium battery. The cathode is
481 made of Lithium metal oxide, i.e. LiCoO₂, the anode is a graphitic carbon cell and the electrolyte
482 can be a non-aqueous solution made of an organic solvent and a dissolved lithium salt or a solid
483 polymer [9].

484 The introduction of carbon cell as anode (Li_xC₆) prevents incidents caused by excessive heating and
485 melting of traditional anode: lithiated carbon has a higher melting point (180°C) [78].

486 During the charging phase, lithium ions are pushed out from the lithium metal oxide (LiMO) and
487 are absorbed by the carbon anode (LiC₆); the vice versa occurs in the discharging phase.

488 The first phase is called “Intercalation” while the second is named “De-Intercalation” [9]. The
489 Electrolyte does not take part in the reaction, it only ensures and facilitates the exchange of ions
490 during the two phases [77]. Typically, the charging (leftward) and discharging (rightward)
491 reactions, respectively at positive and negative electrode, are [9] :



494 The reasons why this technology is considered the best frontier of energy storage are: high energy
495 density (160 ÷ 200 Wh/kg) [9,77], fast response time (milliseconds) [9], low self-discharge rate (5%
496 per month) [11] and high efficiency (up to 97%) [9,79]. Cons regard lifetime and Depth of
497 Discharge. Both are temperature dependent. Aging effect is enhanced by high temperature
498 [12,13,80] . Moreover, this battery requests a complex management system, usually called Battery

499 Management System (BMS). It is an electronic platform which monitors and estimates the battery
500 State of Health (SoH) in real time: it controls the aging effect, checks the performances and
501 detects the End of Life at cell level, in order to prevent cell fail and predict components
502 substitution [77][81][82][83]. This system also protects the battery against overheating, low
503 temperature, overcharge and discharge and provides optimal working conditions (like
504 charging/discharging current and voltage) [78,80,81]. Obviously, such equipment increases the
505 battery's cost.

506 A huge cost decrease in the latest years is highlighted: while in 2009 unit cost was estimated
507 between 900 and 1300 \$/kWh [13], it was reduced to about 600 \$/kWh in 2012 [11] and it ranges
508 between 225 and 800 \$/kWh [84] .

509 This trend is due to latest developments in battery design: over the above-mentioned thermal
510 management [80], research proceeds to enhance power capability by adopting nanoscale
511 materials and to increase specific energy by studying innovative materials for electrode and
512 electrolyte [85–88]. A concrete application of a Lithium-iron-phosphate (LiFePO_4) battery is
513 reported in [89]. Batteries are employed to reduce the fuel consumption of the diesel generators
514 in an oil drilling rig. In this specific case, a major attention is focused on the reactive power: a
515 parallel connected capacitor (the so-called DC-link) is placed between the battery pack and the
516 power inverter, making the battery able to handle both Active and Reactive power. A 175,000 EUR
517 total investment plus 11,400 EUR/year for maintenance has been considered. Employing a
518 proportional State of Charge based energy controller (for generator/battery switch on/off), up to
519 17.69 m^3 of diesel can be saved. The return-of-investment period has been estimated between 1
520 and 2 years (battery life is rated to be 10 years). CO_2 reduction is about 5000t in magnitude. Such
521 results demonstrate how mature this technology is. Moreover, the importance of a good energy
522 management policy is, again, high lined.

523 Lithium-Sulfur battery is emerging as a credible alternative for common lithium ion battery due to
524 high specific energy, low cost, raw material abundance, safety and low environmental
525 impact[85,90].

526 Selenium (Se), which is the congener of Sulfur, has been studied in order to introduce an
527 innovative carbon-based material doped with SeS_x . The composite material, called $\text{SeS}_x/\text{NCPAN}$,
528 should replace the traditional cathode, increasing capacity and lifetime [87] .

529 Dimethylsulfoxide (DMSO) replaces the carbonated based electrolyte in a Lithium-air battery to
530 enhance cycling performances, reducing anode's fast deterioration. A higher (>20%) coulombic
531 efficiency, despite standard Li-air technology, is obtained [86].

532 A new generation of Li-ion battery employs a solid-state electrolyte, composed of garnet-type
533 metal borohydrides, which can improve of seven orders of magnitude the ion exchange due to
534 microcrystalline geometry [88].

535 4. Hydrogen storage

536 In the hydrogen storage technique, the hydrogen is produced using the exceeding energy, then it
537 is stored and eventually the energy is recovered from the stored Hydrogen. The last phase consists
538 in a electrical energy production by using either a traditional internal combustion engine or a fuel
539 cell [7,9,91].

540 Hydrogen has remarkable features as a fuel. It has a High Heating Value (HHV) of 141,8 MJ/kg,
541 which is more than double in comparison to methane. In addition, the fact that it burns in
542 stoichiometric conditions with an air-to-fuel ratio equal to 34.33, coupled with its very wide
543 flammability limits, allows a combustion with a very low fuel consumption. The main drawback
544 emerges considering its density in STP condition, which is very low, namely 0,084 kg/m³. This
545 affects the energy density value, which, despite the great HHV [91]. This factor is crucial, since it
546 marks the difficulty in storing hydrogen by using traditional methods, such as gas compression or
547 liquefaction, and suggests the use of fuel cells in place of internal combustion engine, if a more
548 efficient process is the desired target [9,91].

549 Hydrogen has been object of several studies concerning its applicability as fuel in power plant [92].
550 For instance, in the engine field it has always been considered an attractive “additive”, either for
551 diesel or natural gas, able to increase engine performance and, more important, to reduce
552 gaseous and soot emissions [93–95]. These features, together with the development of innovative
553 combustion control techniques [96,97], and the use of various after-treatment devices [98], are
554 essential for meeting the newest emission standards [99].

555 About 95% of the worldwide hydrogen production involves non-renewable resources. Hydrogen is
556 extracted from natural gas by means of an endothermic process at high temperature
557 (800÷1000°C) in presence of a catalyst. In such technique, called Steam Reforming, natural gas acts
558 both as raw material for hydrogen production and as fuel, since it is burned to increase the
559 temperature of the process. A natural gas amount comprised between 3 and 20% is used to keep
560 alive the reaction. For each ton of hydrogen produced, 2.5 ton of CO₂ are released [91].

561 Hydrogen extraction from coal has been widely investigated. Such a process has a heavier
562 environmental impact in comparison to the extraction from NG (5 Tons of CO₂ are released for
563 each ton of H₂ produced). To contain the environmental impact, either the Pressure Swing
564 Adsorption (PSA) or the Carbon Capture System (CCS) techniques have been developed. CCS

565 enabled plants have higher (22%) Hydrogen cost. To reduce overall H₂ cost, electricity co-
566 production (by gasified coal) has been considered [91].

567 In a relative new technique hydrogen is produced starting from gasoline and diesel fuels. This
568 process, called Partial DeHydrogenation (PDH), leads to a high purity hydrogen (up to 99%) and
569 allows the recover the original fuels. The reaction acts in presence of a catalyst, like Platinum, at
570 400°C and at 0.1 MPa. About 1800 NI/h and 3500 NI/h of Hydrogen for kilogram of catalyst mass
571 are produced respectively form gasoline and diesel. The catalyst life is about 300 hours for
572 gasoline and 29 hours for diesel [100].

573 Hydrogen productions by using water electrolysis and biomass amount to, respectively, the 4%
574 and the 1% of the total production [91]. In Water electrolysis electricity is employed to brake the
575 water molecule bonds, generating oxygen and hydrogen atoms. The production rate is higher in
576 presence of an electrolyte, commonly KOH (which is reusable). The efficiency of this kind of
577 process is high (up to 75%) [91,101] and the purity of the produced hydrogen can reach 99,9%
578 [101,102]. However, its costs are high because of the electricity consumption (about 4.49 kWh/m³
579 are required) and the expensive coated electrodes (Platinum) required in the process. The
580 introduction of a Cobalt phosphate catalyst allowed to decrease the costs [91]. Further
581 development concerned the cathode material: instead of Platinum and other expensive materials,
582 Microbial Electrolysis Cell (MEC) can be used, which employed a macro-porous nickel foam-
583 graphene (NF-graphene) cathode, which provides the diffusion of the respiring bacteria for
584 hydrogen production [103]. Renewable and sustainable resources has to be preferred also
585 because of the energy related cost reduction; micro and small wind turbines (<50 kW) can be used
586 in grid system to feed the electrolyser [102].

587 Furthermore, the solar energy can be involved in the hydrogen production. Four different
588 techniques are usually adopted, namely photovoltaic panels, to feed electrolyser; photo-
589 electrolysis, to split water by photons energy; solar thermal, to exploit thermochemical reactions
590 for thermolysis process; and photobiological generation to provide decomposition of water by
591 microalgae and cyanobacteria activated by solar light [91,101].

592 Recently, Khalilnejad and. Riahy [104] designed a hybrid wind–photovoltaic system for the
593 purpose of hydrogen production through water electrolysis. They analysed three different
594 conditions, consisting respectively in using just wind turbine (WT), photovoltaic (PV) array, and
595 combination of them as power source. The results showed that the combination of WT and PV
596 array was the best choice. The average hydrogen production rate of combined system was 0.0173
597 mol/s (26.2% and 127% more than the other two solutions respectively). On the other hand,

598 average unused power production of combined system was 0.183 kW, namely 3.8% less than the
599 first solution, and 55% more than the second one.

600 The energy management strategy (EMS) to control hybrid system is a crucial aspect that have
601 heavily influence on the overall efficiency and costs. Cau et al. [105] give a practical example with
602 their study about an isolated micro grid powered by a photovoltaic array and a wind turbine and
603 equipped with two different energy storage systems, namely electric batteries and a hydrogen
604 production and storage system. They proposed an EMS that considered the uncertainty due to the
605 intermittent nature of renewable resources and electricity demand. Starting from forecasts of
606 weather conditions and load requirements, the optimal generation scheduling to minimize
607 operating costs and maximize system efficiency with a stochastic approach was proposed. The
608 results showed a reduction of utilization costs of about 15% in comparison to conventional EMS
609 based on the state-of-charge (SOC) of batteries and an increase of the average energy storage
610 efficiency.

611 As well as for fossil fuel, the hydrogen production processes from biomass rely on thermochemical
612 or biological reactions [91,106–108]. Glycerol, which is a product of biodiesel industries, is often
613 used to produce hydrogen by various techniques: steam reforming (SR) -comparable to the fossil
614 fuel case, partial oxidation reforming (POR) , autothermal reforming (ATR), aqueous phase
615 reforming (APR) and supercritical water reforming (SCWR) [91,106]. Moreover, microalgae are
616 often preferred to cultivation biomasses due to the higher growth rate, a more efficient solar
617 energy conversion, the higher nutrient acquisition, and the ability to grow under severe conditions
618 [91,107].

619 Hydrogen can be also produced from bio-oil too. The process is based on the sorption enhanced
620 steam reforming (SESR) of acetic acid, a bio-oil compound, and by using dolomite as CO₂ sorbent.
621 The resulting H₂ has a 99.8% purity and it is suitable for cell application without further
622 purifications [108].

623 The traditional methods in gas storing consist in compression and liquefaction. The production of
624 pressurized hydrogen at 200 bar is the most commonly employed technique. Despite the high
625 storage pressure, the energy content per weight remain low, since the very low density.
626 Therefore, in order to enhance the hydrogen quantity, the storing pressure is usually increased up
627 to 700 bar, but the adoption of more resistant tanks is not the only side effect. Unfortunately, the
628 compression cost also increases proportionally. In comparison, the liquefaction process
629 guarantees a better storage in terms of energy density, but this technique needs a cryogenic
630 system, since in order to keep the hydrogen in liquid state it is necessary to reach a temperature

631 of 20.4 K. Obviously, such a process is quite inefficient due to the unavoidable thermal losses and
632 the high cost for the cryogenic system [13,109].

633 Zhang et al. [110] provided a comprehensive evaluation of the performance of a grid-tied
634 microgrid, consisting of a PV system, a hydrogen fuel cell stack, a PEM electrolyzer, and a
635 hydrogen tank. The surplus electricity was stored as hydrogen, which was supplied to the fuel cell
636 stack to generate heat and power as needed. They found that the emission and the service quality
637 were higher when the fuel cell stack was employed.

638 Another example concerning hybrid renewable energy-based power plants with hydrogen as the
639 intermediate energy storage medium is provided by Valverde et al. [111]. In their study, six
640 operation modes were defined according to plant topology and the possibility of operating
641 electrolyzer and fuel cell at steady-power or partial load, allowing to conclude that certain modes
642 resulted more appropriate from technical and practical standpoints when they are implemented in
643 a real plant. In particular, modes operating the fuel cell and electrolyzer at variable power showed
644 better efficiency indicators but at higher cost, sometimes inadmissibly high. In contrast, modes
645 working at steady power had reduced degradation costs, with the drawback of lower efficiency.

646 An innovative way for the hydrogen storage is based on the chemisorption ability of Metal
647 hydrides [112]. Metal hydrides are alloys of cerium, lanthanum and nickel (Ce-La-Ni) [113],
648 magnesium borohydride $\text{Mg}(\text{BH}_4)_2$ [114], magnesium hydride with zirconium oxide and single-
649 walled carbon nanotubes [115]. The storage process consists in thermochemical reactions that
650 occur between the gaseous hydrogen and the solid materials, which are able to change its
651 crystalline structure during the adsorption and the desorption phases. Specifically, the adsorption
652 reaction is exothermic, while the desorption is endothermic, so a thermal control system is
653 required [13]. The whole process depends on the activation energy, the thermal conductivity, the
654 pressure and the temperature [113–115]. In comparison with traditional methods, this technology
655 is safer, requires lower service costs, is more compact, has greater energy content per weight and
656 guarantees higher efficiency, while the reactions kinetic is very fast provides rapid hydrogen
657 release and fast response. However, metal hydrides have some drawbacks: apart the
658 aforementioned thermal management, their cost is high and the hydrogen content per weight,
659 even if it is greater than that obtainable from the traditional methods, is still low.

660 In order to reduce the influence of the thermal management, metal hydrides can be ~~endowed~~
661 coupled with a thermic storage based on phase change material (PCM) which exploits ~~the~~ the material
662 latent heat in place of external heat sources [116]. Rhodium-silver alloys ($\text{Ag}_x\text{Rh}_{x-1}$ with $0 \leq x \leq 1$)
663 show important properties in hydrogen storing where the adsorption potential depends on alloy
664 composition and electronic structure configuration [117].

665 Natural clay porous Nano-material is cheap, biocompatible, very durable and has a high hydrogen
666 storage capability. An example of natural clay is represented by the acid treated halo site clay
667 nanotubes (A-HNTs) doped with hexagonal boron nitride nanoparticles (h-BN): up to 0.22%
668 hydrogen in weight can be stored in pristine nanotubes; increasing nanoparticles up to 5% the
669 stored hydrogen quantity can reach 2.88wt.% [112].

670 Clathrate hydrates are solid compound whose crystalline structure is made of water molecules.
671 The particular shape of crystals guarantees the presence of cavities, which can be filled with
672 particular gases, called gas hydrates: these gases have low molecular weight comparable to
673 methane, carbon dioxide and hydrogen. The clathrate can resist at high pressure at room
674 temperature in solid state.- The efficiency relies on cavities size [118].

675 5. Assessment and comparison

676 Among the treated systems there are several differences regarding the characterizing parameters
677 of an ESS such as the energy capacity, the power rating, the efficiency, the lifetime, the discharge
678 the time, the maturity and the cost.

679 A comparison between the various systems described above is provided with the aim to better
680 clarify the fundamental differences existing among them. The analysis focuses, for each storage
681 system, on the aforementioned characteristics and, at last, resumes them in the Table 4 obtaining
682 a useful and simple overview. In this section, the hydrogen energy storage is neglected because of
683 its great number of alternative techniques, with remarkable differences in terms of approaches
684 and features.

685 *Power and energy*

686 The Power rating represents the maximum power that the system can handle during the charge
687 and discharge phases, while the energy is often associated to the system capacity.

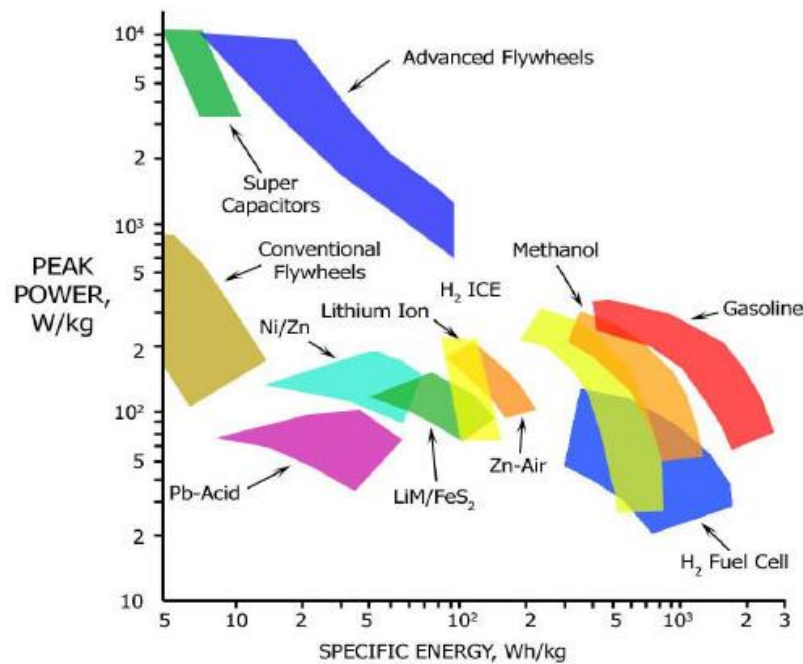


Figure 12 - Power rating, Ragone Chart [119]

Usually, the specific power and energy are used to compare different technologies. Plotting the specific energy versus the specific power, the Ragone Chart is obtained and it is reported in Figure 12. Both the axes use logarithmic scale and each area refers to a particular storage system. The devices with a faster response, such as the supercapacitors or the flywheels, have a great specific power and a low specific energy while fuels, fossil or renewable, which have a lower response time, presents a higher specific energy but a lower specific power.

Efficiency

The cycle efficiency is defined as the ratio between the discharged energy (supplied to loads) and the energy needed to restore the initial state of the charge. The efficiency takes into account the various losses typical of each system, either mechanical losses for PH, CAES and FES or ohmic and chemical-related losses for BES.

Discharge time

ESSs have discharge times varying from few milliseconds to many hours. Consequently, it is possible to sort the storage systems:

- Short discharge time: less than 1 hour, typical value for flywheels and supercapacitors;
- Medium discharge time: up to 10 hour, involving small-scale CAES and batteries;
- Long discharge time: greater than 10 hours, usually for PHS and large-scale CAES.

Lifetime

This parameter refers to the number of charge-discharge cycles that the system can handle without considerably losing its power, energy and efficiency capabilities. Generally, mechanical

710 storage systems have longer lifetime, while other systems are affected by chemical deterioration
711 and even temperature-dependent phenomena.

712 *Cost*

713 The cost comprehends both the installation and the ordinance and maintenance cost. Many
714 technologies have low capital cost but require many maintenance during lifetime. The unit costs
715 are often used in the analysis: in particular power [\$/kW] and energy cost [\$/kWh]. In fact, specific
716 power and energy can be quite different, as shown in Ragone Chart, so, energy and power cost
717 can be different as well.

718 *Technical Maturity*

719 The maturity is referred to the experience acquired in the use of a specific technology, to the level
720 of commercialization, the technical risks and the related economic benefits. It is then possible to
721 divide the ESSs in:

- 722 • Mature technologies: PHS find application in energy storage since XX century;
- 723 • Developed technologies: mature technologies from the technical point of view and
724 commercially available, but large-scale applications are not widespread, such as lithium-ion
725 battery or flywheel;
- 726 • Developing technologies: technologies under development and not commercially mature.

727 A comparison among different energy storage systems is reported in Table 4.

728

729 Table 4 Comparison among different energy storage systems

Technology	Specific Power [W/kg]	Specific Energy [Wh/kg]	Power Rating [MW]	Efficiency [%]	Discharge Time	Lifetime [years]	Power Cost [\$ /kW]	Energy Cost [\$ /kWh]	Technical Maturity
PHS	-	0.5 ÷ 1.5 [9]	4100 [10] <3000 [9]	Up to 87% [10,11]	1÷24+ h [10,11]	40 [9]	500-1500 [10]	10-20 [10]	Mature [12], [11]
CAES	-	30 ÷ 60 [9]	10 ÷ 110, 290 [28]	42% [9] 70% [28]	1÷24+ h [28]	40 [11]	400÷1500 [11], [28]	2÷120 [28] 2÷50 [12]	Mature for large app [28]
FES	400 ÷ 1500 [9,12]	5÷100[13] 10÷80 [9] 100÷130 [41]	0.25 [9] [37] 0.5 [14]	90% [13,14]	Milliseconds÷15 min [12] 15 s ÷ 15 min [9]	>20[11] 15 [12]	250÷350 [9] [12]	1000÷5000 [9] , [12]	Mature for low speed [37]
Flow Battery	150 ÷ 160 [9]	10÷30 [11]	0.5÷100 [11]	85%[11]	2÷12 h [9] Seconds ÷ 10 h	5÷10 [11] 5÷15 [12]	600÷1500[11]	100 [64] 150÷1000 [12]	Developing [11]
Lithium Battery	150 ÷ 315 [9]	160 ÷200 [9][77]	0.1÷100 [9] 0.5 [79]	up to 97% [9][79]	Minutes ÷ Hours [9]	5÷15 [12] 28 [79]	4000 [9] [11]	350÷700 [80]	Developed [80] [81]

730

731 6. Conclusions

732 In the recent past, little is being done to create and develop the research sector and the industrial
733 sector about energy storage. On the contrary, these topics are the most important to radically
734 change the way in which the energy production sector could be organised. So a long term planning
735 to promote research is desirable in every Government of the nations and it should ensure that
736 energy storage is seen as a key ingredient in the energy policy landscape and is very much part of
737 the policy roadmap of every country. For example given, in the Obama age, energy storage
738 industry is now an active in US with an estimated annual investment of over 500 Million of dollars.
739 Energy storage systems (ESSs) are a fundamental requirement for innovative, and future, energy
740 production by means of renewable resources. This scenario should become part of an emerging
741 “global industry” with a potential business approximatively of a trillion dollar.

742 So this paper has provided an overview of the most promising ESSs, performing technical and
743 economic features, with the purpose of providing the state of the art and promoting the research
744 in this field. The always rising energy demand with the greenhouse gasses reduction goal makes
745 renewable sources the new frontier of energy production. However, the behaviour of such sources
746 is often unpredictable and, in the most general case, the availability almost never satisfies the
747 demand. Moreover, a transition to a “grid” energy system is expected to come, enhancing the
748 efficiency of the distribution process. This explains why an ESS that can significantly increase the
749 global efficiency of the system is duplicable. Therefore, ESS represents a crucial device for the
750 future of the energy production.

751 In this paper the most spread and promising technologies have been reviewed. A detailed
752 description of their characteristics together with an extensive analysis of the state of the art was
753 provided. Finally, a comparison between all the different solutions considered throughout the
754 present analysis was reported.

755 A storage system that is at the same time mature, durable, efficient, cheap, with a wide power
756 range can only be obtained by matching different technologies, i.e., flywheels and batteries often
757 find application in automotive or stationary plants while PHS or CAES are usually employed for
758 large size energy storage.

759 The analysis of the value of the specific power and energy provides a useful comparison. In fact,
760 the systems with huge capacity and power rating and long discharge time, like PHS and CAES, have
761 low values of specific energy. Conversely, FESs, which have fast discharge time, provide high
762 power, but can store a low quantity of energy. Flow batteries represent an important in-
763 perspective solution because they are composed of numerous modules: capacity and power rating
764 can be adjusted varying the number and dimension of such modules. Unfortunately, this versatile

765 technology is still in the developing phase. Hydrogen energy storage relies on different techniques
766 and solutions, and the great part of them is still in a developing phase, such as carbon nanotubes
767 or clathrate hydrates, while others, such as metal hydrides, are more mature, but they need to be
768 optimized before being commercially available. The traditional compression systems of the
769 hydrogen are still the more commonly adopted technology, in particular when matched with
770 electrolyser or fuel cell systems. Finally, lithium batteries showed a decisive development in the
771 last few years in a way that their power rating has been enhanced, their lifetime has got longer,
772 their efficiency has been increased and their costs has been reduced.
773

774	<i>Nomenclature</i>	
775	<i>BESs</i>	<i>Battery Energy Storage system</i>
776	<i>BMS</i>	<i>Battery Management System</i>
777	<i>CAES</i>	<i>Compressed Air Energy Storage</i>
778	<i>CNT</i>	<i>Carbon Nano Tubes</i>
779	<i>DoD</i>	<i>Depth of Discharge</i>
780	<i>ED</i>	<i>Energy Density</i>
781	<i>EE</i>	<i>Energetic Efficiency</i>
782	<i>ESS</i>	<i>Energy Storage system</i>
783	<i>FES</i>	<i>Flywheel Energy Storage</i>
784	<i>PaT</i>	<i>Pump as Turbine</i>
785	<i>PH(S)</i>	<i>Pumped Hydroelectric (Storage)</i>
786	<i>RFB</i>	<i>Redox Flow Battery</i>
787	<i>SES</i>	<i>Supercapacitor Energy Storage</i>
788	<i>SMES</i>	<i>Superconducting Magnetic Energy Storage</i>
789	<i>SoH</i>	<i>State of Health</i>
790	<i>T&D</i>	<i>Transmission and Distribution</i>
791	<i>Mtoe</i>	<i>Million Tonnes of Oil Equivalent</i>
792		

793 References

- 794 [1] Catalano LA, De Bellis F, Amirante R, Rignanese M. An Immersed Particle Heat Exchanger for
795 Externally Fired and Heat Recovery Gas Turbines. *J Eng Gas Turbines Power*
796 2011;133:32301.
- 797 [2] Amirante R, Tamburrano P. High Temperature Gas-to-Gas Heat Exchanger Based on a Solid
798 Intermediate Medium. *Adv Mech Eng* 2015;6:353586–353586. doi:10.1155/2014/353586.
- 799 [3] Amirante R, Tamburrano P. Novel, cost-effective configurations of combined power plants
800 for small-scale cogeneration from biomass: Feasibility study and performance optimization.
801 *Energy Convers Manag* 2015;97:111–20. doi:10.1016/j.enconman.2015.03.047.
- 802 [4] Amirante R, Clodoveo ML, Distaso E, Ruggiero F, Tamburrano P. A tri-generation plant
803 fuelled with olive tree pruning residues in Apulia: An energetic and economic analysis.
804 *Renew Energy* 2016;89:411–21.
- 805 [5] Abdeshahian P, Lim JS, Ho WS, Hashim H, Lee CT. Potential of biogas production from farm
806 animal waste in Malaysia. *Renew Sustain Energy Rev* 2016;60:714–23.
807 doi:10.1016/j.rser.2016.01.117.
- 808 [6] Poh PE, Tan DT, Chan E-S, Tey BT. Current Advances of Biogas Production via Anaerobic
809 Digestion of Industrial Wastewater. *Adv. Bioprocess Technol.*, Cham: Springer International
810 Publishing; 2015, p. 149–63. doi:10.1007/978-3-319-17915-5_9.
- 811 [7] Ibrahim H, Ilinca A, Perron J. Energy storage systems—Characteristics and comparisons.
812 *Renew Sustain Energy Rev* 2008;12:1221–50. doi:10.1016/j.rser.2007.01.023.
- 813 [8] Singh S, Singh M, Chandra S. Feasibility study of an islanded microgrid in rural area
814 consisting of PV , wind , biomass and battery energy storage system. *Energy Convers Manag*
815 2016;128:178–90. doi:10.1016/j.enconman.2016.09.046.
- 816 [9] Luo X, Wang J, Dooner M, Clarke J. Overview of current development in electrical energy
817 storage technologies and the application potential in power system operation. *Appl Energy*
818 2015;137:511–36. doi:10.1016/j.apenergy.2014.09.081.
- 819 [10] Rehman S, Al-Hadhrami LM, Alam MM, Rehman S, Al-Hadhrami LM, Alam MM. Pumped
820 hydro energy storage system: A technological review. *Renew Sustain Energy Rev*
821 2015;44:586–98.

- 822 [11] Kousksou T, Bruel P, Jamil A, El Rhafiki T, Zeraouli Y. Energy storage: Applications and
823 challenges. *Sol Energy Mater Sol Cells* 2014;120:59–80. doi:10.1016/j.solmat.2013.08.015.
- 824 [12] Chen H, Cong TN, Yang W, Tan C, Li Y, Ding Y. Progress in electrical energy storage system: A
825 critical review. *Prog Nat Sci* 2009;19:291–312. doi:10.1016/j.pnsc.2008.07.014.
- 826 [13] Hadjipaschalis I, Poullikkas A, Efthimiou V. Overview of current and future energy storage
827 technologies for electric power applications. *Renew Sustain Energy Rev* 2009;13:1513–22.
828 doi:10.1016/j.rser.2008.09.028.
- 829 [14] M. Urbani, Corsi N. Confronto tra diversi sistemi di accumulo di energia. 6° Congr. Naz.
830 CIRIAF, 2006.
- 831 [15] Bueno C, Carta JA. Wind powered pumped hydro storage systems, a means of increasing
832 the penetration of renewable energy in the Canary Islands. *Renew Sustain Energy Rev*
833 2006;10:312–40. doi:10.1016/j.rser.2004.09.005.
- 834 [16] Liu Y, Jiang C, Shen J, Hu J, Luo Y. Coordination of hydro units with wind power generation
835 based on RAROC. *Renew Energy* 2015;80:783–92. doi:10.1016/j.renene.2015.02.062.
- 836 [17] Kusakana K. Feasibility analysis of river off-grid hydrokinetic systems with pumped hydro
837 storage in rural applications. *Energy Convers Manag* 2015;96:352–62.
838 doi:10.1016/j.enconman.2015.02.089.
- 839 [18] Development of Pump Turbine for Seawater Pumped- Storage Power Plant. *Hitachi Rev*
840 1998;47.
- 841 [19] Theodoropoulos P, Zervos A, Betzios G. Hybrid systems using pump-storage implementation
842 in Ikaria island Title. *Int. Conf. Renew. Energies Islands–Towards 100% RES Supply*, 2001.
- 843 [20] Mason IG. Comparative impacts of wind and photovoltaic generation on energy storage for
844 small islanded electricity systems. *Renew Energy* 2015;80:793–805.
845 doi:10.1016/j.renene.2015.02.040.
- 846 [21] Sarasúa JI, Pérez-Díaz JI, Wilhelmi JR, Sánchez-Fernández JÁ. Dynamic response and
847 governor tuning of a long penstock pumped-storage hydropower plant equipped with a
848 pump-turbine and a doubly fed induction generator. *Energy Convers Manag* 2015;106:151–
849 64. doi:10.1016/j.enconman.2015.09.030.
- 850 [22] Deyou L, Hongjie W, Gaoming X, Ruzhi G, Xianzhu W, Zhansheng L. Unsteady simulation and

851 analysis for hump characteristics of a pump turbine model. *Renew Energy* 2015;77:32–42.
852 doi:10.1016/j.renene.2014.12.004.

853 [23] Jain S V, Swarnkar A, Motwani KH, Patel RN. Effects of impeller diameter and rotational
854 speed on performance of pump running in turbine mode. *Energy Convers Manag*
855 2015;89:808–24.

856 [24] Amirante R, Andrea Catalano L, Tamburrano P. Thrust Control of Small Turbojet Engines
857 Using Fuzzy Logic: Design and Experimental Validation. *J Eng Gas Turbines Power* 2012.
858 doi:10.1115/1.4007372.

859 [25] Xu Y, Zhou J, Xue X, Fu W, Zhu W, Li C. An adaptively fast fuzzy fractional order PID control
860 for pumped storage hydro unit using improved gravitational search algorithm. *Energy*
861 *Convers Manag* 2016;111:67–78. doi:10.1016/j.enconman.2015.12.049.

862 [26] Yao E, Wang H, Wang L, Xi G, Maréchal F. Thermo-economic optimization of a combined
863 cooling, heating and power system based on small-scale compressed air energy storage.
864 *Energy Convers Manag* 2016;118:377–86. doi:10.1016/j.enconman.2016.03.087.

865 [27] Milazzo A. Optimization of the configuration in a CAES-TES system 2008.

866 [28] Luo X, Wang J, Dooner M, Clarke J, Krupke C. Overview of Current Development in
867 Compressed Air Energy Storage Technology. *Energy Procedia* 2014;62:603–11.
868 doi:10.1016/j.egypro.2014.12.423.

869 [29] Zhao P, Wang J, Dai Y. Thermodynamic analysis of an integrated energy system based on
870 compressed air energy storage (CAES) system and Kalina cycle. *Energy Convers Manag*
871 2015;98:161–72. doi:10.1016/j.enconman.2015.03.094.

872 [30] M S, FA S, PY L. Modeling and control of an open accumulator Compressed Air Energy
873 Storage (CAES) system for wind turbines. *Appl Energy* 2015;137:603–16.

874 [31] Pei P, Korom SF, Ling K, He J, Gil A. Thermodynamic impact of aquifer permeability on the
875 performance of a compressed air energy storage plant. *Energy Convers Manag*
876 2015;97:340–50. doi:10.1016/j.enconman.2015.03.072.

877 [32] Basbous T, Younes R, Ilinca A, Perron J. Optimal management of compressed air energy
878 storage in a hybrid wind-pneumatic-diesel system for remote area's power generation.
879 *Energy* 2015;84:267–78.

- 880 [33] Pete C, McGowan JG, Jaslanek W. Evaluating the Underwater Compressed Air Energy
881 Storage Potential in the Gulf of Maine. 2014.
- 882 [34] Yao E, Wang H, Liu L, Xi G. A Novel Constant-Pressure Pumped Hydro Combined with
883 Compressed Air Energy Storage System. *Energies* 2014;8:154–71. doi:10.3390/en8010154.
- 884 [35] Guo H, Xu Y, Chen H, Zhou X. Thermodynamic characteristics of a novel supercritical
885 compressed air energy storage system. *Energy Convers Manag* 2016;115:167–77.
886 doi:10.1016/j.enconman.2016.01.051.
- 887 [36] Liu H, He Q, Borgia A, Pan L, Oldenburg CM. Thermodynamic analysis of a compressed
888 carbon dioxide energy storage system using two saline aquifers at different depths as
889 storage reservoirs. *Energy Convers Manag* 2016;127:149–59.
890 doi:10.1016/j.enconman.2016.08.096.
- 891 [37] Bolund B, Bernhoff H, Leijon M. Flywheel energy and power storage systems. *Renew Sustain*
892 *Energy Rev* 2007;11:235–58. doi:10.1016/j.rser.2005.01.004.
- 893 [38] Conteh MA, Nsofor EC. Composite flywheel material design for high-speed energy storage. *J*
894 *Appl Res Technol* 2016;14:184–90. doi:10.1016/j.jart.2016.04.005.
- 895 [39] Ramli MAM, Hiendro A, Twaha S. Economic analysis of PV/diesel hybrid system with
896 flywheel energy storage. *Renew Energy* 2015;78:398–405.
897 doi:10.1016/j.renene.2015.01.026.
- 898 [40] Ren G, Ma G, Cong N. Review of electrical energy storage system for vehicular applications.
899 *Renew Sustain Energy Rev* 2015;41:225–36. doi:10.1016/j.rser.2014.08.003.
- 900 [41] Dhand A, Pullen K. Review of battery electric vehicle propulsion systems incorporating
901 flywheel energy storage. *Int J Automot Technol* 2015;16:487–500. doi:10.1007/s12239-015-
902 0051-0.
- 903 [42] Moro D, Cavina N, Trivić I, Ravaglioli V. Guidelines for Integration of Kinetic Energy Recovery
904 System (KERS) based on Mechanical Flywheel in an Automotive Vehicle, 2010.
905 doi:10.4271/2010-01-1448.
- 906 [43] Li W, Chau KT, Ching TW, Wang Y, Chen M. Design of a High-speed Superconducting
907 Bearingless Machine for Flywheel Energy Storage Systems. *IEEE Trans Appl Supercond*
908 2014;25:1–1. doi:10.1109/TASC.2014.2367008.

- 909 [44] Mukoyama S, Matsuoka T, Hatakeyama H, Kasahara H, Furukawa M, Nagashima K, et al.
 910 Test of REBCO HTS Magnet of Magnetic Bearing for Flywheel Storage System in Solar Power
 911 System. *IEEE Trans Appl Supercond* 2015;25:1–4. doi:10.1109/TASC.2014.2363044.
- 912 [45] Amodeo SJ, Chiacchiarini HG, Solsona JA, Busada CA. High-performance sensorless
 913 nonlinear power control of a flywheel energy storage system. *Energy Convers Manag*
 914 2009;50:1722–9. doi:10.1016/j.enconman.2009.03.024.
- 915 [46] Hamzaoui I, Bouchafaa F, Talha A. Advanced control for wind energy conversion systems
 916 with flywheel storage dedicated to improving the quality of energy. *Int J Hydrogen Energy*
 917 2016;41:20832–46. doi:10.1016/j.ijhydene.2016.06.249.
- 918 [47] Zhang X, Zhang Z, Pan H, Salman W, Yuan Y, Liu Y. A portable high-efficiency
 919 electromagnetic energy harvesting system using supercapacitors for renewable energy
 920 applications in railroads. *Energy Convers Manag* 2016;118:287–94.
 921 doi:10.1016/j.enconman.2016.04.012.
- 922 [48] Dubal DP, Ayyad O, Ruiz V. Hybrid energy storage: the merging of battery and
 923 supercapacitor chemistries. *Chem Soc Rev* 2015;44:1777–90. doi:10.1039/C4CS00266K.
- 924 [49] Xu C, Xu B, Gu Y, Xiong Z, Sun J, Zhao XS. Graphene-based electrodes for electrochemical
 925 energy storage. *Energy Environ Sci* 2013;6:1388. doi:10.1039/c3ee23870a.
- 926 [50] Zhang Y-Z, Wang Y, Cheng T, Lai W-Y, Al. E. Flexible supercapacitors based on paper
 927 substrates: a new paradigm for low-cost energy storage. *Chem Soc Rev* 2015;44:5181–99.
 928 doi:10.1039/C5CS00174A.
- 929 [51] Chen T, Dai L. Carbon nanomaterials for high-performance supercapacitors. *Mater Today*
 930 2013;16:272–80. doi:10.1016/j.mattod.2013.07.002.
- 931 [52] Cakici M, Kakarla RR, Alonso-Marroquin F. Advanced electrochemical energy storage
 932 supercapacitors based on the flexible carbon fiber fabric-coated with uniform coral-like
 933 MnO₂ structured electrodes. *Chem Eng J* 2017;309:151–8. doi:10.1016/j.cej.2016.10.012.
- 934 [53] Ise T, Kita M, Taguchi A. A Hybrid Energy Storage With a SMES and Secondary Battery. *IEEE*
 935 *Trans Appiled Supercond* 2005;15:1915–8. doi:10.1109/TASC.2005.849333.
- 936 [54] Pullano SA, Fiorillo AS, Morandi A, Ribani PL. Development of an innovative
 937 superconducting magnetic energy storage system. 2015 AEIT Int. Annu. Conf., IEEE; 2015, p.

938 1–3. doi:10.1109/AEIT.2015.7415280.

939 [55] Pullano S, Bianco MG, Critello C, Laganà F, Menniti D, Ruberto F, et al. Biomass Plant and
940 Sensors Network for Process Monitoring and Energy Storage in a Superconducting Magnetic
941 Device. *Saf Technog Environ* 2014;6:28. doi:10.7250/ste.2014.012.

942 [56] Ray PK, Mohanty SR, Kishor N. Proportional-integral controller based small-signal analysis of
943 hybrid distributed generation systems. *Energy Convers Manag* 2011;52:1943–54.
944 doi:10.1016/j.enconman.2010.11.011.

945 [57] Bensmaine F, Bachelier O, Tnani S, Champenois G, Mouni E. LMI approach of state-feedback
946 controller design for a STATCOM-supercapacitors energy storage system associated with a
947 wind generation. *Energy Convers Manag* 2015;96:463–72.
948 doi:10.1016/j.enconman.2015.02.059.

949 [58] Cunha Á, Martins J, Rodrigues N, Brito FP. Vanadium redox flow batteries: a technology
950 review. *Int J Energy Res* 2015;39:889–918. doi:10.1002/er.3260.

951 [59] Pan F, Wang Q. Redox Species of Redox Flow Batteries: A Review. *Molecules*
952 2015;20:20499–517. doi:10.3390/molecules201119711.

953 [60] Pezeshki AM, Clement JT, Veith GM, Zawodzinski TA, Mench MM. High performance
954 electrodes in vanadium redox flow batteries through oxygen-enriched thermal activation. *J*
955 *Power Sources* 2015;294:333–8. doi:10.1016/j.jpowsour.2015.05.118.

956 [61] Lin J, Shang Y, Lin X, Yang L, Yu A. Study on Nitrogen-Doped Carbon Nanotubes for
957 Vanadium Redox Flow Battery Application 2016;11:665–74.

958 [62] Chen J-Z, Liao W-Y, Hsieh W-Y, Hsu C-C, Chen Y-S. All-vanadium redox flow batteries with
959 graphite felt electrodes treated by atmospheric pressure plasma jets. *J Power Sources*
960 2015;274:894–8. doi:10.1016/j.jpowsour.2014.10.097.

961 [63] Ulaganathan M, Jain A, Aravindan V, Jayaraman S, Ling WC, Lim TM, et al. Bio-mass derived
962 mesoporous carbon as superior electrode in all vanadium redox flow battery with
963 multicouple reactions. *J Power Sources* 2015;274:846–50.
964 doi:10.1016/j.jpowsour.2014.10.176.

965 [64] Dennison CR, Agar E, Akuzum B, Kumbur EC. Enhancing Mass Transport in Redox Flow
966 Batteries by Tailoring Flow Field and Electrode Design. *J Electrochem Soc* 2015;163:A5163–

- 967 9. doi:10.1149/2.0231601jes.
- 968 [65] Jia C, Cheng Y, Ling X, Wei G, Liu J, Yan C. Sulfonated poly(Ether Ether
969 Ketone)/functionalized carbon nanotube composite membrane for vanadium redox flow
970 battery applications. *Electrochim Acta* 2015;153:44–8. doi:10.1016/j.electacta.2014.11.123.
- 971 [66] Xi J, Li Z, Yu L, Yin B, Wang L, Liu L, et al. Effect of degree of sulfonation and casting solvent
972 on sulfonated poly(ether ether ketone) membrane for vanadium redox flow battery. *J*
973 *Power Sources* 2015;285:195–204. doi:10.1016/j.jpowsour.2015.03.104.
- 974 [67] Cao L, Kong L, Kong L, Zhang X, Shi H. Novel sulfonated polyimide/zwitterionic polymer-
975 functionalized graphene oxide hybrid membranes for vanadium redox flow battery. *J Power*
976 *Sources* 2015;299:255–64. doi:10.1016/j.jpowsour.2015.09.026.
- 977 [68] Pezeshki AM, Tang ZJ, Fujimoto C, Sun C-N, Mench MM, Zawodzinski TA. Full Cell Study of
978 Diels Alder Poly(phenylene) Anion and Cation Exchange Membranes in Vanadium Redox
979 Flow Batteries. *J Electrochem Soc* 2015;163:A5154–62. doi:10.1149/2.0201601jes.
- 980 [69] Xi X, Ding C, Zhang H, Li X, Cheng Y, Zhang H. Solvent responsive silica composite
981 nanofiltration membrane with controlled pores and improved ion selectivity for vanadium
982 flow battery application. *J Power Sources* 2015;274:1126–34.
983 doi:10.1016/j.jpowsour.2014.10.160.
- 984 [70] Li W, Liang Z, Lu Z, Tao X, Liu K, Yao H, et al. Magnetic Field-Controlled Lithium Polysulfide
985 Semiliquid Battery with Ferrofluidic Properties. *Nano Lett* 2015;15:7394–9.
986 doi:10.1021/acs.nanolett.5b02818.
- 987 [71] Ding Y, Zhao Y, Yu G. A Membrane-Free Ferrocene-Based High-Rate Semiliquid Battery.
988 *Nano Lett* 2015;15:7094–9. doi:10.1021/acs.nanolett.5b01224.
- 989 [72] Zhao Y, Ding Y, Li Y, Peng L, Byon HR, Goodenough JB, et al. A chemistry and material
990 perspective on lithium redox flow batteries towards high-density electrical energy storage.
991 *Chem Soc Rev* 2015;44:7968–96. doi:10.1039/c5cs00289c.
- 992 [73] Janoschka T, Martin N, Martin U, Friebe C, Morgenstern S, Hiller H, et al. An aqueous,
993 polymer-based redox-flow battery using non-corrosive, safe, and low-cost materials. *Nature*
994 2015;527:78–81. doi:10.1038/nature15746.
- 995 [74] Li N, Wang Y, Tang D, Zhou H. Integrating a Photocatalyst into a Hybrid Lithium-Sulfur

- 996 Battery for Direct Storage of Solar Energy. *Angew Chemie* 2015;127:9403–6.
997 doi:10.1002/ange.201503425.
- 998 [75] Zakeri B, Syri S. Electrical energy storage systems: A comparative life cycle cost analysis.
999 *Renew Sustain Energy Rev* 2015;42:569–96. doi:10.1016/j.rser.2014.10.011.
- 1000 [76] Gong K, Ma X, Conforti KM, Al. E. A zinc–iron redox-flow battery under \$100 per kW h of
1001 system capital cost. *Energy Environ Sci* 2015;8:2941–5. doi:10.1039/C5EE02315G.
- 1002 [77] Baker J. New technology and possible advances in energy storage. *Energy Policy*
1003 2008;36:4368–73. doi:10.1016/j.enpol.2008.09.040.
- 1004 [78] Abada S, Marlair G, Lecocq A, Petit M, Sauvant-Moynot V, Huet F. Safety focused modeling
1005 of lithium-ion batteries: A review. *J Power Sources* 2016;306:178–92.
1006 doi:10.1016/j.jpowsour.2015.11.100.
- 1007 [79] Graditi G. Technical and economical assessment of distributed electrochemical storages for
1008 load shifting applications: An Italian case study 2016.
- 1009 [80] Panchal S, Dincer I, Agelin-Chaab M, Fraser R, Fowler M. Thermal modeling and validation of
1010 temperature distributions in a prismatic lithium-ion battery at different discharge rates and
1011 varying boundary conditions. *Appl Therm Eng* 2016;96:190–9.
1012 doi:10.1016/j.applthermaleng.2015.11.019.
- 1013 [81] Rahman MA, Anwar S, Izadian A. Electrochemical model parameter identification of a
1014 lithium-ion battery using particle swarm optimization method. *J Power Sources*
1015 2016;307:86–97. doi:10.1016/j.jpowsour.2015.12.083.
- 1016 [82] Berecibar M, Gandiaga I, Villarreal I, Omar N, Van Mierlo J, Van den Bossche P. Critical
1017 review of state of health estimation methods of Li-ion batteries for real applications. *Renew*
1018 *Sustain Energy Rev* 2016;56:572–87. doi:10.1016/j.rser.2015.11.042.
- 1019 [83] Patsios C, Wu B, Chatzinikolaou E, Rogers DJ, Wade N, Brandon NP, et al. An integrated
1020 approach for the analysis and control of grid connected energy storage systems. *J Energy*
1021 *Storage* 2016;5:48–61. doi:10.1016/j.est.2015.11.011.
- 1022 [84] Renewable Energy Agency I. IRENA Battery Storage Report 2015 2015.
- 1023 [85] Zhang Z, Wang G, Lai Y, Li J. A freestanding hollow carbon nanofiber/reduced graphene
1024 oxide interlayer for high-performance lithium–sulfur batteries. *J Alloys Compd*

- 1025 2016;663:501–6. doi:10.1016/j.jallcom.2015.11.120.
- 1026 [86] Togasaki N, Momma T, Osaka T. Enhanced cycling performance of a Li metal anode in a
 1027 dimethylsulfoxide-based electrolyte using highly concentrated lithium salt for a
 1028 lithium–oxygen battery. *J Power Sources* 2016;307:98–104.
 1029 doi:10.1016/j.jpowsour.2015.12.123.
- 1030 [87] Guo S-P, Li C-X, Chi Y, Ma Z, Xue H-G. Novel 3-D network SeSx/NCPAN composites prepared
 1031 by one-pot in-situ solid-state method and its electrochemical performance as cathode
 1032 material for lithium-ion battery. *J Alloys Compd* 2016;664:92–8.
 1033 doi:10.1016/j.jallcom.2015.12.208.
- 1034 [88] Brighi M, Schouwink P, Sadikin Y, Cerny R. ChemInform Abstract: Fast Ion Conduction in
 1035 Garnet-Type Metal Borohydrides $\text{Li}_3\text{K}_3\text{Ce}_2(\text{BH}_4)_{12}$ and $\text{Li}_3\text{K}_3\text{La}_2(\text{BH}_4)_{12}$. *ChemInform*
 1036 2016;47:no-no. doi:10.1002/chin.201615009.
- 1037 [89] Pavković D, Sedić A, Guzović Z. Oil drilling rig diesel power-plant fuel efficiency
 1038 improvement potentials through rule-based generator scheduling and utilization of battery
 1039 energy storage system. *Energy Convers Manag* 2016;121:194–211.
 1040 doi:10.1016/j.enconman.2016.05.022.
- 1041 [90] Marinescu M, Zhang T, Offer GJ. A zero dimensional model of lithium–sulfur batteries
 1042 during charge and discharge. *Phys Chem Chem Phys* 2016;18:584–93.
 1043 doi:10.1039/C5CP05755H.
- 1044 [91] Hosseini SE, Wahid MA. Hydrogen production from renewable and sustainable energy
 1045 resources: Promising green energy carrier for clean development. *Renew Sustain Energy*
 1046 *Rev* 2016;57:850–66. doi:10.1016/j.rser.2015.12.112.
- 1047 [92] Pilavachi PA, Stephanidis SD, Pappas VA, Afgan NH. Multi-criteria evaluation of hydrogen
 1048 and natural gas fuelled power plant technologies. *Appl Therm Eng* 2009;29:2228–34.
 1049 doi:10.1016/j.applthermaleng.2008.11.014.
- 1050 [93] Hora TS, Shukla PC, Agarwal AK. Particulate emissions from hydrogen enriched compressed
 1051 natural gas engines. *Fuel* 2015:1–7. doi:10.1016/j.fuel.2015.11.035.
- 1052 [94] Sofianopoulos A, Assanis DN, Mamalis S. Effects of Hydrogen Addition on Automotive Lean-
 1053 Burn Natural Gas Engines: Critical Review. *J Energy Eng* 2015;142:E4015010.

- 1054 [95] Verma G, Prasad RK, Agarwal RA, Jain S, Agarwal AK. Experimental investigations of
1055 combustion, performance and emission characteristics of a hydrogen enriched natural gas
1056 fuelled prototype spark ignition engine. *Fuel* 2016;178:209–17.
1057 doi:10.1016/j.fuel.2016.03.022.
- 1058 [96] Amirante R, Casavola C, Distaso E, Tamburrano P. Towards the Development of the In-
1059 Cylinder Pressure Measurement Based on the Strain Gauge Technique for Internal
1060 Combustion Engines Operating Principles of the Proposed Strain. *SAE - Int.*, 2015.
1061 doi:10.4271/2015-24-2419.Copyright.
- 1062 [97] Shimasaki Y, Kobayashi M, Sakamoto H, Ueno M, Hasegawa M, Yamaguchi S, et al. Study on
1063 engine management system using in-cylinder pressure sensor integrated with spark plug.
1064 2004.
- 1065 [98] Myung CL, Park S. Exhaust nanoparticle emissions from internal combustion engines: A
1066 review. *Int J Automot Technol* 2012;13:9–22.
- 1067 [99] Amirante R, Distaso E, Tamburrano P, Reitz RD. Measured and Predicted Soot Particle
1068 Emissions from Natural Gas Engines. *SAE - Int.*, 2015. doi:10.4271/2015-24-2518.Copyright.
- 1069 [100] Gianotti E, Taillades-Jacquín M, Reyes-Carmona Á, Taillades G, Rozière J, Jones DJ. Hydrogen
1070 generation via catalytic partial dehydrogenation of gasoline and diesel fuels. *Appl Catal B*
1071 *Environ* 2016;185:233–41. doi:10.1016/j.apcatb.2015.12.015.
- 1072 [101] Yilmaz F, Balta MT, Selbaş R. A review of solar based hydrogen production methods. *Renew*
1073 *Sustain Energy Rev* 2016;56:171–8. doi:10.1016/j.rser.2015.11.060.
- 1074 [102] Dixon C, Reynolds S, Rodley D. Micro/small wind turbine power control for electrolysis
1075 applications. *Renew Energy* 2016;87:182–92. doi:10.1016/j.renene.2015.09.055.
- 1076 [103] Cai W, Liu W, Han J, Wang A. Enhanced hydrogen production in microbial electrolysis cell
1077 with 3D self-assembly nickel foam-graphene cathode. *Biosens Bioelectron* 2016;80:118–22.
1078 doi:10.1016/j.bios.2016.01.008.
- 1079 [104] Khalilnejad A, Riahy GH. A hybrid wind-PV system performance investigation for the
1080 purpose of maximum hydrogen production and storage using advanced alkaline
1081 electrolyzer. *Energy Convers Manag* 2014;80:398–406.
1082 doi:10.1016/j.enconman.2014.01.040.

- 1083 [105] Cau G, Cocco D, Petrollese M, Knudsen Kær S, Milan C. Energy management strategy based
1084 on short-term generation scheduling for a renewable microgrid using a hydrogen storage
1085 system. *Energy Convers Manag* 2014;87:820–31. doi:10.1016/j.enconman.2014.07.078.
- 1086 [106] Schwengber CA, Alves HJ, Schaffner RA, da Silva FA, Sequinel R, Bach VR, et al. Overview of
1087 glycerol reforming for hydrogen production. *Renew Sustain Energy Rev* 2016;58:259–66.
- 1088 [107] Aziz M. Integrated hydrogen production and power generation from microalgae. *Int J*
1089 *Hydrogen Energy* 2016;41:104–12. doi:10.1016/j.ijhydene.2015.10.115.
- 1090 [108] MV G, J F, C P, D C, F R. Production of fuel-cell grade H₂ by sorption enhanced steam
1091 reforming of acetic acid as a model compound of biomass-derived bio-oil. *Appl Catal B*
1092 *Environ* 2016;184:64–76.
- 1093 [109] Chilev C, Lamari FD. Hydrogen storage at low temperature and high pressure for application
1094 in automobile manufacturing. *Int J Hydrogen Energy* 2016;41:1744–58.
1095 doi:10.1016/j.ijhydene.2015.11.099.
- 1096 [110] Zhang L, Xiang J. The performance of a grid-tied microgrid with hydrogen storage and a
1097 hydrogen fuel cell stack. *Energy Convers Manag* 2014;87:421–7.
1098 doi:10.1016/j.enconman.2014.07.045.
- 1099 [111] Valverde L, Pino FJ, Guerra J, Rosa F. Definition, analysis and experimental investigation of
1100 operation modes in hydrogen-renewable-based power plants incorporating hybrid energy
1101 storage. *Energy Convers Manag* 2016;113:290–311. doi:10.1016/j.enconman.2016.01.036.
- 1102 [112] Muthu RN, Rajashabala S, Kannan R. Synthesis, characterization of hexagonal boron nitride
1103 nanoparticles decorated halloysite nanoclay composite and its application as hydrogen
1104 storage medium. *Renew Energy* 2016;90:554–64. doi:10.1016/j.renene.2016.01.026.
- 1105 [113] Schur DV, Gabdullin MT, Bogolepov VA, Veziroglu A, Zaginaichenko SY, Savenko AF, et al.
1106 Selection of the hydrogen-sorbing material for hydrogen accumulators. *Int J Hydrogen*
1107 *Energy* 2016;41:1811–8. doi:10.1016/j.ijhydene.2015.10.011.
- 1108 [114] Goumri-Said S, Ahmed R, Kanoun MB. Density-functional theory study of high hydrogen
1109 content complex hydrides Mg(BH₄)₂ at low temperature. *Renew Energy* 2016;90:114–9.
1110 doi:10.1016/j.renene.2015.12.044.
- 1111 [115] Hwang S-J, Chuang Y-S. Enhanced hydrogen storage properties of MgH₂ co-catalyzed with

1112 zirconium oxide and single-walled carbon nanotubes. J Alloys Compd 2016;664:284–90.
1113 doi:10.1016/j.jallcom.2015.12.243.

1114 [116] Mâad HB, Miled A, Askri F, Nasrallah SB. Numerical simulation of absorption-desorption
1115 cyclic processes for metal-hydrogen reactor with heat recovery using phase-change
1116 material. Appl Thermal Eng 2016;96:267–76.

1117 [117] Yayama T, Ishimoto T, Koyama M. Theoretical investigation of hydrogen absorption
1118 properties of rhodium–silver alloys. J Alloys Compd 2016;662:404–8.
1119 doi:10.1016/j.jallcom.2015.12.008.

1120 [118] Papadimitriou NI, Tsimpanogiannis IN, Economou IG, Stubos AK, Al. E. Evaluation of the
1121 Efficiency of Clathrate Hydrates in Storing Energy Gases. J Phys Conf Ser 2015;640:12026.
1122 doi:10.1088/1742-6596/640/1/012026.

1123 [119] Ghoniem AF. Needs, resources and climate change: Clean and efficient conversion
1124 technologies. Prog Energy Combust Sci 2011;37:15–51. doi:10.1016/j.pecs.2010.02.006.

1125